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DANNYBAY - SEISMIC EFFECTS

From 0.8 - 340 km $a(g) = \frac{0.75}{W(\text{tons})} \times 10^{-2.9} R^{-2}$

Measured values

R (km)	Acc (g) (10 ⁻²)
0.76	4.7, 4.7, 6.8
1.22	2.8, 6.6, 9.4
2.13	1.1, 2.1, 3.2

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Event Name

Yield

Medium

Mississippi

110

SWT

Merrimac

DELETED

Slightly consol. all

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LENL

Dried salmon

Event	W(kg)	Loc.	DOB (ft)
Abatanum		U2L	750
Clearwater	DELETED	U12C	1800
Tornillo		U9ag	500

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$$R = \frac{403}{70} = 5.757$$
$$R = \sqrt[2]{.16}$$

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DATE ✓ Name location
 21, on 5 Dec
 Nov 21 * DELETED Greys U9ax, 1050
 31

* Open or other on 14th

* Dec 6
 Jan 16
 Jan 30
 Feb 6
 Jan 96
 Mar 4
 ?

DELETED

~~Klickitat U10e, 1625
 Oconto U9ay, 875
 Payette U2ab, 750
 Flat U20a, 2050
 Fore U10i, 1600
 U9a0
 Turf U10c, 1673
 Slice U7a, 220'~~

LASU

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* Klickitat - 2/6 per Cont. T.B. * 72(5) LLNL

71

Con. Test Bull # 72

Date Shot	W	Depth/Hole
Nov 21 or Dec 5	GREYS	U9ax, 1000
Jan 16	Fore	U9ao, 1625
Feb 6	Klickitat	U10e, 1625

DELETED

4X163

CTB # 72 - 29X63 -

W [REDACTED]

Date	W	Name	Location/DOB
11/21 or 12/5		Greys	U9ax, 1000'
> 1/6/64		Oconto	U9ay, 875
1/16		Fore	U9ao, 1625
2/6		Klickitat	U10e, 1625
2/27		Alva	u2j, 550

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Throw-out -

Nothing on R/A aspects

Lacrosse - (W 40 KT) Land Surface Bunt.
WT 1354 Reducing F/O studies

WT 1319 - Land F.O Studies
Prog 2.65 Evaluate B.S. transport

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111

1967 12 10

Baker - Howland Study -

Seminole - Opn Redwing - DELETED

- For the opn - Surveys @ H+1 to H+4

H+4 to H+8

D+1 & D+2.

13.7 ± 1.5

~~12.4~~ kt

Water tank - ground surface

Eniwetok.

per WT 1366-

630,000 m³/hr on shot island at

Reentry held up 2 days

Helicopter reentry to bunker not affected

Earlier shot I m³/hr

5 May 9,900 31 days

28 40

31 May 70

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$$1 \text{ kt} = 1200 \text{ r/hr} @ \text{H+1/mi}^2$$

La Crosse - DELETED Redwing

5 May - 40 kt - Ground surface - Eniwetok
+17 ft.

1 m/hr @ H+4 — 30,200 on Island

at edge (outer) of crater - H+1
57000 r/hr.

$$A_2 = A_1 e^{-1.2}$$

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WT 1311 -

Any decay - 1.1 - 1.3

Some affected by rain leaching:

A ~ 50% of what
it would be from
decay alone.

Detectors in pipe: Collimation factor 1.4

LINK

WT 1311 - Proj 2.2 - REDWING RAD SAFETY

Residual & Radiation: $I_t = I_0 t^{-1.2}$

$$r = \int_{t_1}^{t_2} I_t dt = 5I_0 (t_1^{-0.2} - t_2^{-0.2})$$

Decay curves for Cherokee, Juni, Hatched, Navajo, Ilwa.

"Beach Ball" Crater residual detector used; Calibration problem? 50000 r/hr @ H+6.
No measurements (except beach ball) at 4/mi

WT 942 - CASTLE RAD SAFE.

Mentions wave effect
Decay curves - See next pg -
Craters

WT 913.

Castle - δ vs T
51R for 1st 25m
1.28 decay between H+1 & H+12
70000 r/hr for G2

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WT 912.

Spectral response of gup \rightarrow uncertainty
Decay rates for room < 1 generally
Reason not known

WT 1311

001 2000

Potd Max. (in/linear cr ter)

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1500 r/hr @ H+4 (ex

15MT

DELETED

on reef

131

DELETED

11MT

DELETED

on barge. H+4 extra 2000 r/hr in crater

DELETED

Keon - 100 DELETED KT

DELETED

on ground. 5000 r/hr @ H+4 in crater.

There were samples taken from some craters

WT1366

ha Croese: H+4 on Shot Island
30000 m/hr

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4 (extr.)
craters
K.F.
craters

W-942 - Initial Hel. 'vey 50-1000' altitude
at H+4 hrs.

Shot 1 - Land - 15 MT - DELETED
Rpt incl. A at a no. of location (rem)

Shot 3 - Land - 100-150 KT
"Small sand dunes around crater
were washed away by
Crater A - 5000 r/hr at H+4

WT1366 - Work done in Mike Crater for Apoc.
A - 4-5 r/hr @ ?

Helicopter surveys at H+2 H+4
"detached" "H+6
& succeeding days.
DELETED

Zuni Shot is land H+4 > 25000 ^{ms/hr}
Dakota DELETED H+4 ~ 5000 ^{ms/hr}.

WT1344 - Edges of Choppers of Probes converted
to 3' land values.

Conversion includes:
Collimation
Depth of Mining in Ocean
Air Absorption

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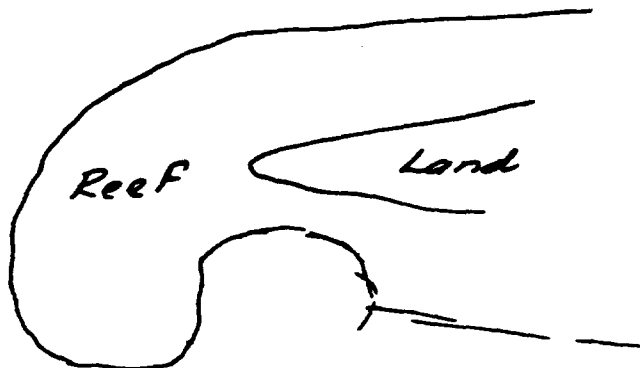
Effect of Sodin 25
Just outside
Crater A : H+1
57000 ms/hr - Lacrosse
13000 - Zuni
Mohawk, not Zuni

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WT1317 - Very little of value.

CASTLE I (WT 920) (Crater Study)

$W_T = 14.5 \text{ MT}$; ~~DELETED~~ On Reef under very shallowly.
 On D+6 - A 10' above water 25-75 m/hr
 "Much higher" on nearby land.
 No lip above water.



WT942

1500 r/hr on adjacent (sw) island. @ H+4

Debris radius - 2-3 mi

CASTLE II ~~DELETED~~

$W_T = 11 \text{ MT}$, ~~DELETED~~

Barge

$D_{H+4} \approx 2000 \text{ r/hr}$ (in crater area)

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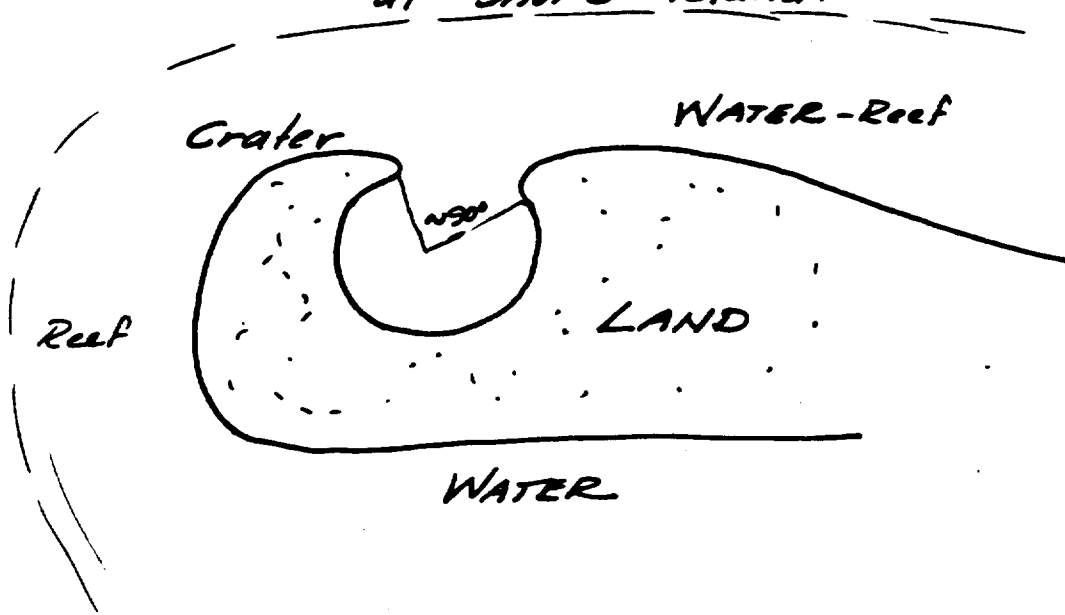
CASTLE 3 (WT 920 Gates unwey)

D+24 - A ~ 1500-3500 m/hr on lip
50 m/hr 10' above water

Shot 4 had been fired between
Shot 3 and D+24. Shot 4 wave
had flooded C3 lip.

There was a lip.

WT942. Shot 4 did not significantly > P.A.
at Shot 3 island.



WT942- Koon- ~~DELETED~~ Castle 3. 130KT all F.
5000 r/hr @ H+4 in crater.
Samples taken fr. some craters.

Castle 4 ~~DELETED~~
Barge in center of lagoon
H 7 MT = WT

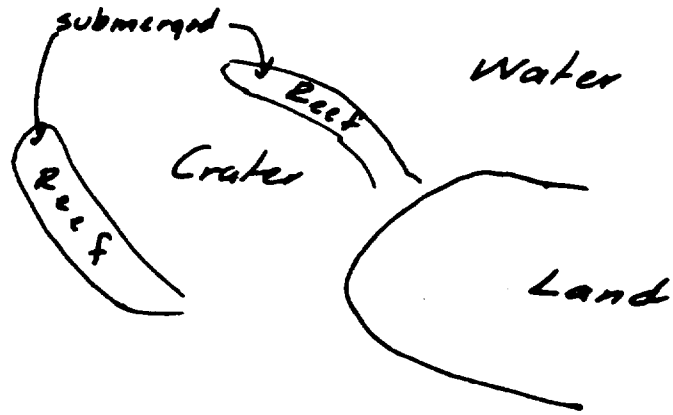
~~DELETED~~

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Nearest land ~ 3 mi
D+4 on nearest land ~ 1400 r/hr

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Zuni : 3.5 MT Total; **DELETED**
 WT1307 - Breaching of crater permitted
 - reentry on D+6

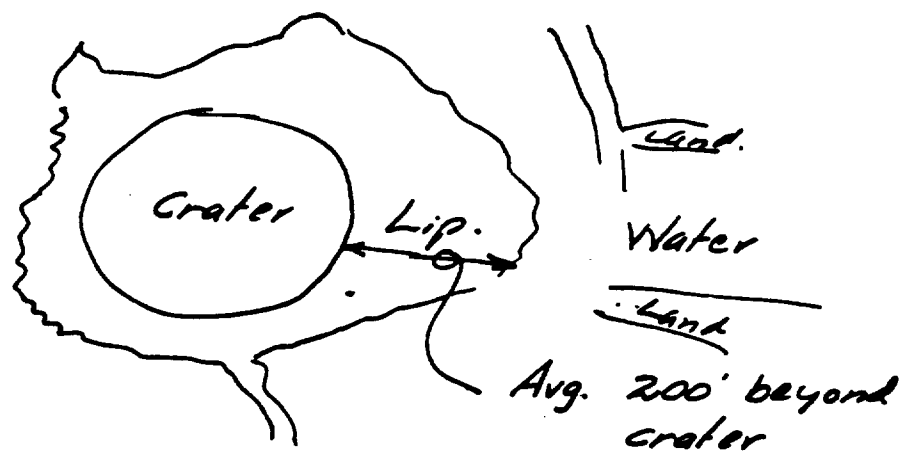


WT1366 H+4 - W_T . 3.5 MT
 25000 m/h **DELETED**
 on shot island
 75000 m/h @ H+4 on Able (~25 mi.)

WT1311 - Beachball ~~see~~ measurement
 50000 r/h @ H+6 in crater.

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Lacrosse - no breaching - 40kt; hob = 17'
2' water over shot reef at Zero time.
Lip ~15' high



WT 1366 - H+4 on shot island 30000r/hr

JASON MINKLER. See notes.

WT 1344 - 57000 r/hr at outer lip - H+1

WT 1319 - 57000 r/hr @ H+1 was isolated
Gen. level 1600-4800 r/hr @ H+1.

Tide had washed reef twice between
shot & readings.

Dmax - 6000 - 8000 r/hr @ H+1.

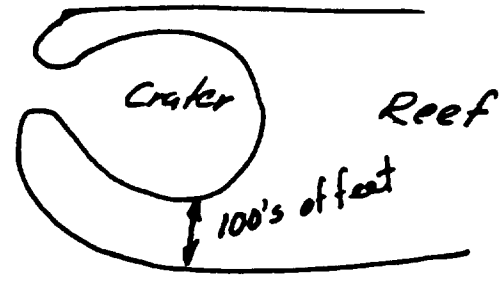
$\delta \approx 1.36$ avg.

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10031 0'66

CACTUS.

Unwashed wt 1609 (Water few ft deep)
∴ D should be down.



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TEINA

DH11 \approx 1500- / hr on islands
2 mi distant.

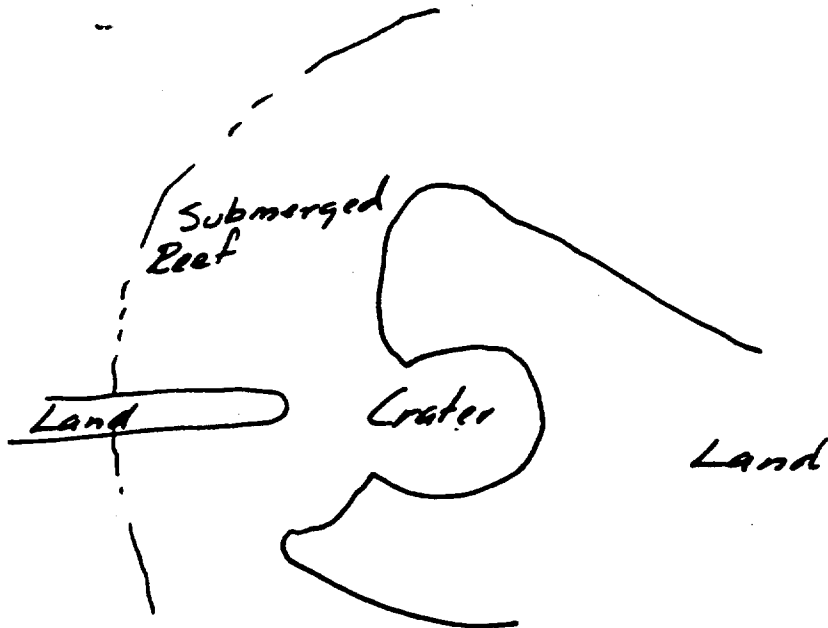
Reef shot. Barge, shallow water.

~ 4.7 MT ,

DELETED

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Seminole. 13.5kt.
Surf Water Tank



1366 - 630 r/hr @ H+4 on adjacent island.

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TE'NA -

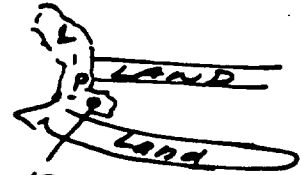
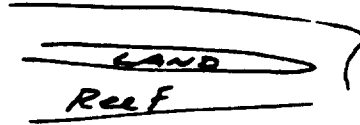
Shallow water barge slot

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36 Tower. on Land.

WT 1344



13200 r/hr @ H+1

Based on H₂O₂ readings

H+1 around crater 8°-13000 r/hr

Areas of high readings not submerged.

WT1366 - 1450 r/hr @ H+4 on Sho + Isl.

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2001 1007

JCH

BL 616 FOOT
WT 1344

DELETED

200 Tower

WT 1366 - $D_{H.4} = 360 \text{ v/hr}$

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Eric

WT 1344

DELETED

300' Tower

WT 1366 - @ H+4 D = 200 r/hr.

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FLATHEAD (TS 285)
WT1344 -

DELETED

Bunge

WT1366 -

H+4 - ~40 r/hr.

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PANUTE '58A EQPMT VULNERABILITY

Gnome:

Acc = 5 g. safe

For deep soil; hard rock shot

$$a = .53 W^{.54} R^{-1.4}$$

$$R^{1.4} = \frac{.53 W^{.54}}{a} \approx .1 W^{.54}$$

$$R = (.1 W^{.54})^{.7} = .2 W^{.38}$$

$$R_{170} = .2 \times 7 = 1.4 \text{ mi} \approx 7500'$$

$$R_{500} = .2 \times 10.5 = 2.1 \approx 11000'$$

$$R_{1000} = .2 \times 14 = 2.8 = 15000'$$

$$R_{1500} = .2 \times 16 = 3.2 = 17000'$$

For rock/shallow soil; hard rock shot; say
Terrain coef = 2

$$a = \frac{.53}{2} W^{.54} R^{-1.4}$$

$$R = (R \text{ from above}) \times (.5)^{.7} \approx .6 R \text{ from above}$$

$$R'_{170} = 4500$$

$$R'_{500} = 7,000$$

$$R'_{1000} = 9,000$$

$$R'_{1500} = 10,000$$

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Velocity: Say 150 cm/sec.

For deep alluvium, hard rock shot: v

$$v = 1.7 W^{.67} R^{-1.5} \quad \text{in/sec, mi, kt}$$

$$R^{1.5} = \frac{1.7}{v} W^{.67}$$

$$R = \left[\frac{1.7 W^{.67} \times 2.54}{150} \right]^{.67} = .1 W^{.44}$$

(cont on page 25) 29

BILBY: Say safe motion = $\frac{2}{3}$ actual Bilby motion
 $\approx \frac{2}{3} g$ w/ proper shock mtg of eqpt.
 $R^{1.4} = \frac{.53}{2} W^{.54}$ for deep alluvium.

$$R = .27^{.7} W^{.38} = .4 W^{.23} = \text{Twice Gnome R}$$

~~Half~~
Twice

- $\therefore R_{170} = 14,500'$
- $R_{500} = 25000 - 22000$
- $R_{1000} = 25000$
- $R_{1500} = 34,000$

Using 3g (Bilby. acc.) ($R = 1.4 \times \text{Gnome R}$)

- $R_{170} = 11000$
- $R_{500} = 18000$
- $R_{1000} = 22000$
- $R_{1500} = 25000$

Using Tern. Coef = 2.

R' still = $2 \times \text{Gnome } R'$

- $R_{170} = 9000$
- $R_{500} = 14000$
- $R_{1000} = 18000$
- $R_{1500} = 21000$

Bilby Velocity (Say 70 cm/sec)

$$R' = \left[\frac{1.7 W^{.67}}{27.5} \right]^{.67} = .15 W^{.46}$$

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$R = 1\frac{1}{2}$ times R from pg 25.

- $R_{170} = 10000$
- $R_{500} = 17000$
- $R_{1000} = 22000$
- $R_{1500} = 26,000$

$$R = .1W^{.44}$$

$$R_{170} = .95 \text{ mi} \approx 5000'$$

$$R_{500} = 1.6 \approx 8500$$

$$R_{1000} = 2.1 \approx 11,000$$

$$R_{1500} = 2.5 \approx 13000$$

— from Gnome vel.

Occupied Trlrs.

$$V = 30 \text{ cm/sec.} \approx 12 \text{ ips}$$

$$V = 1.7W^{.67}R^{-.45}$$

$$R = \left(\frac{1.7W^{.67}}{V}\right)^{.67} \approx (.14W^{.67})^{.67} = .27W^{.44}$$

$$R_{170} = .27 \times 9.5 \times 5280 = 13,500'$$

$$R_{500} = \downarrow 17 \downarrow = 24,000'$$

$$R_{1000} = \downarrow 21 \downarrow = 30,000$$

$$R_{1500} = \downarrow 25 \downarrow = 35,500$$

Acc. 3g on Rock (T.C. = 2)

$$a = .53W^{.54}R^{-1.4}$$

$$R^{1.4} = \frac{.53W^{.54}}{2a} = \frac{.53W^{.54}}{6} \approx (.09W^{.54})$$

$$R \approx .18W^{.38} \text{ mi} = 950W^{.38} \text{ ft}$$

$$R_{170} = \cancel{18} 950 \times 7.2 = 7000$$

$$R_{500} \downarrow 11 = 10500$$

$$R_{1000} \downarrow 14 = 13500$$

$$R_{1500} \downarrow 17 = 16000$$

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