

410915

C L S

VERSION

)ELETED

· WT-1318

**OPERATION REDWING**—PROJECT 2.64

# FALLOUT LOCATION and DELINEATION by AERIAL SURVEYS (U)

R. T. Graveson M. E. Cassidy H.D. LeVine

New York Operations Office Atomic Energy Commission New York, New York

ELASSIFICATION CANCELLED WITH DELETIONS BY AUTHORITY OF DOE/ OC US DOE ARCHIVES 826 U.S. ATOMIC ENERGY RG\_\_\_\_COMMISSION Collection DOS MCCraw Job 1320 Box 22 IRICTED Folder MRA7 Redwing - Fallout Location of Delivertion by Aerial Surv This document restricted data as Act of 1954. defined in th WT-1318 al or the disclo Its tra its in any manner to an unauta co on is prohibited. pel 3

## FOREWORD

This report presents the final results of one of the projects participating in the military-effect programs of Operation Redwing. Overall information about this and the other military-effect projects can be obtained from WT-1344, the "Summary Report of the Commander, Task-Onit 3." This technical summary includes: (1) tables listing each detonation with its yield, type, environment, meteorological conditions, etc.; (2) maps showing shot locations; (3) discussions of results by programs; (4) summaries of objectives, procedures, results, etc., for all projects; and (5) a listing of project reports for the military-effect programs.

DOE ARCHIVES

### ABSTRACT

The objectives were to: (1) survey the gamma radiation from fallout-contaminated ocean areas by means of aerial detectors and (2) from the aerial detectors make air-absorption measurements so that the data might be related to the dose rates at 3 feet above the sea.

Radiation detectors were mounted in P2V-5 aircraft that surveyed the ocean areas of expected fallout after Shots Cherokee, Zuni, Flathead, Navajo, Mohawk, and Tewa. A control center coordinated all air and surface radiation-survey activities to insure complete coverage of the fallout area. The contamination densities in the delineated areas were related to the percentage of the total yield that produced fission products. Gamma-isodose plots were prepared from data obtained during Shots Zuni, Flathead, Navajo, and Tewa. No fallout could be located following Shot Cherokee and only on atoll islands after Shot Mohawk.

Zuni, a land-surface shot, contaminated 13,400 naut mi<sup>2</sup> of ocean with 48 percent of its fissionproduct yield.

Navajo, a water-surface shot, contaminated 10,500 naut  $mi^2$  with 50 percent of the fissionproduct yield. After Flathead, another water-surface shot, the outer boundary could not determined because of contamination of project aircraft on D + 1 day by airborne radioactive material that resulted in a high background. However, extrapolated values indicate 29 percent of its fission-product yield was present as fallout in the local area. The fallout from the watersurface shots was concentrated primarily in the more remote areas, and a relatively small amount fell close to ground zero.

Tewa, a reef shot, contaminated 43,500 naut mi<sup>2</sup> of ocean with 28 percent of the fission-product yield.

Helicopters and P2V-5 aircraft were used to gather data for air-absorption measurements.

The aerial-survey technique may be used directly for radiological surveys over land. Over the sea, the depth of mixing of the fallout in the water volume must be determined before the survey results may be converted to equivalent land-fallout contours and contamination-density distributions. Data on depth of mixing was obtained from samples of sea water collected by the U.S. Naval Radiological Defense Laboratory and the Scripps Institute of Oceanography. Repeated aerial surveys provided information on the stability of the contaminated volume.

DOE ARCHIVES

### PREFACE

Patrol Squadron ONE, U.S. Navy, operated the aircraft used for the aerial surveys. The author gratefully acknowledges the diligence and high professional competence which contributed so much to the project's operations.

Commander Kelly, USN, was the Air Officer on the staff of Commander, Task Group 7.3. His efforts were responsible for the fulfillment of the project's aircraft requirements.

Members of the Health and Safety Laboratory, U.S. Atomic Energy Commission, who participated in the field operations, and whose contributions are gratefully acknowledged are I. Whitney, G. Hamada, S. Tarras and T. French of the Analytical Branch, H. Sadowski and F. Wilson of the Instruments Branch and K. O'Brien of the Radiation Branch.

6

### DOE ARCHIVES

¥

# CONTENTS

FOREWORD	4
ABSTRACT	5
PREFACE	6
CHAPTER 1 INTRODUCTION	11
1.1 Objectives	11
1.2 Background	11
1.3 Theory	12
1.3.1 Fallout Contamination of a Water Volume	12
1.3.2 Fallout Contamination of a Land Surface	13
1.3.3 Radioactive Decay	14
1.3.4 Distribution of Fallout	15
CHAPTER 2 PROCEDURE	16
2.1 Shot Participation	16
2.2 Operations	
2.2.1 Aerial Surveys	16
2.2.2 Altitude Absorption	19
2.3 Instrumentation	19
2.3.1 Aerial Survey	19
2.3.2 Altitude Absorption	20
2.4 Required Data	20
2.4.1 Distribution of Contamination in the Sea	23
2.4.2 Altitude Absorption	23
2.4.3 Stability of Contaminated Area	23
CHAPTER 3 RESULTS	24
3.1 Instrumentation Performance	24
3.1.1 Aerial Surveys	24
3.1.2 Altitude Absorption	24
3.2 Altitude Absorption Measurements	25
3.3 Distribution of Fallout	28
3.3.1 Shot Cherokee	28
3.3.2 Shot Zuni	28
3.3.3 Shot Flathead	31
3.3.4 Shot Mohawk	35
3.3.5 Shot Navajo	35
3.3.6 Shot Tewa	45
3.4 Samples of Contaminated Sea Water	45
3.4.1 Gamma Radiation as a Function of Beta Activity	45
3.4.2 Depth of Mixing	DOE ARCHIVES
CHAPTER 4 DISCUSSION	55
4.1 Operational Performance	55
7	

7,

.



3.8 Flir pattern, Shot Zuni, D+2 days	32
3.9 Fligne pattern. Shot Zuni, D+3 days	
3.10 Flight pattern. Shot Flathead. D-day	34
3.11 Flight pattern. Shot Flathead D+1 day	36
3.12 Atoll readings Shot Mohawk D+1 day	
3.13 Flight nattern Shot Mohawk D+1 day	
3.14 Special aerial survey Shot Navaio D-3 days	30
3 15 Aerial survey ("flush" flight nattern) Shot Navajo D-	2 days =
3 16 Shin nattern derived from data received from Project	262 40
3.17 Flight pattern Shot Navajo Deday	
3 18 Flight pattern, Shot Navajo, D+1 day	42
3 19 Flight pattern, Shot Navajo, D+2 days	
3 20 Flight pattern, Shot Tawa D-1 day	
3.21 Flight pattern, Shot Tewa, D-1 day	
3.22 Flight pattern, Shot Tewa, D-day D-1 day	
3 23 Flight pattern, Shot Tewa, D+2 days	40
3 24 Flight pattern, Shot Tewa, D+3 days	
3 25 Flight pattern Shot Tewa D+4 days	51
3.26 Effective denth of mixing for fallout in the sea	
4.1 Distribution of fallout contamination. Shots Flathead an	d Navajo
4.2 Distribution of fallout contamination, Shots Zuni and Te	$\mathbf{W}^{2} = \mathbf{F}^{2} $
8.1 Radium gamma-radiation calibration Ton Hat detector	
B? Freirgy dependence of dose-rate response injustic and	
sodium indide detectors	6A
C 1 Badiation attenuation over land	69
C 2 Radiation attenuation over water-	
C:2 Radiation attendation over water	00
I) I Camma doce rate at 3 test related to surface beta activity	rity TA
D.1 Gamma dose rate at 3 feet related to surface beta activ	vity74
D.1 Gamma dose rate at 3 feet related to surface beta activ D.2 Depth of mixing from sea water samples. Shots Flathe	vity74 ad and Navajo 75
D.1 Gamma dose rate at 3 feet related to surface beta activ D.2 Depth of mixing from sea water samples, Shots Flathe D.3 Depth of mixing from sea water samples, Shot Tewa -	vity74 ad and Navajo 75 75
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta activ</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> </ul>	rity74 ad and Navajo 75 75
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta activ</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> </ul>	vity 74 ad and Navajo 75 75
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li> </ul>	rity 74 ad and Navajo 75 75
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 17 26
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 17 17 26 26 31
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 75
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 75 75 75 75 75 75 7
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active D.2 Depth of mixing from sea water samples, Shots Flathe D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 75 75 75 75 75 75 7
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 26 31 31 31 35 45 53
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 75 75 75 75 75 75 7
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 75 75 75 75 75 75 7
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active D.2 Depth of mixing from sea water samples, Shots Flathe D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 75 75 75 75 75 75 7
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	vity       74         ad and Navajo       75         75       75         75       75         75       75         75       75         75       75         76       75         77       75         75       75         76       75         77       75         77       75         75       75         75       75         75       75         75       75         76       75         77       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75 </td
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity       74         ad and Navajo       75         75       75         75       75         75       75         75       75         75       75         75       75         76       75         77       75         75       75         75       75         76       75         77       75         75       75 </td
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity       74         ad and Navajo       75         75       75         75       75         75       75         75       75         75       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75 </td
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity       74         ad and Navajo       75         75       75         75       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         75       75         75       75         76       75         77       75         75       75         75       75         76       75         77       73         78       73         79       73         71       75         73       73         74       73         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75 </td
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity       74         ad and Navajo       75         75       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         77       75         77       75         77       75         77       75         77       75         77       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75         75       75 </td
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity 74 ad and Navajo 75 75 75 75 75 75 75 70 70 75 75 70 75 75 70 
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity       74         ad and Navajo       75         75       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       75         77       76         77       71         76       71
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flathe</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	$2^{i}$ ty 74         ad and Navajo 75         75         75         75         75         75         75         75         75         75         75         75         75         75         76         77         76         77         76         77         73         74         75         75         75         75         76         77         75         76         70         71         71
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flather</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	$2^{i}$ ty 74         ad and Navajo 75         76         77         70         71         72         74         72
<ul> <li>D.1 Gamma dose rate at 3 feet related to surface beta active</li> <li>D.2 Depth of mixing from sea water samples, Shots Flather</li> <li>D.3 Depth of mixing from sea water samples, Shot Tewa -</li> <li>TABLES</li> <li>2.1 Summary of Project Operations</li></ul>	rity       74         ad and Navajo       75         75       75         75       75         75       75         76       75         77       75         75       75         76       75         77       75         75       75         76       71         77       71         78       73

**9**-10

:



### Chapter I INTRODUCTION

#### 1.1 OBJECTIVES

The objectives were to: (1) survey the gamma radiation from fallout-contaminated ocean areas using an airborne detector and (2) make air-absorption measurements so that the data from the airborne detector might be related to the dose rates at 3 feet above the sea.

#### 1.2 BACKGROUND

During Operation Ivy, the USAEC Health and Safety Laboratory (HASL) carried out a program of aerial surveys of the islands outside the Eniwetok Proving Ground (Reference 1). No major fallout occurred on any of these land surfaces. Traces of contamination were clearly discernible from the air, indicating the feasibility of aerial surveys. However, with the meager basic data then available, it was not possible to determine whether the contamination from a multimegaton shot, namely, Shot Mike, was primarily deposited as local fallout or remained in the upper levels of the atmosphere.

A similar program of aerial surveys was organized for Operation Castle (Reference 2). It was expanded to include monitoring installations at certain selected islands outside the Eniwetok Proving Ground. Shot 1 deposited appreciable fallout on the monitoring installation at Rongerik. Although heavy fallout was thus documented from a multimegaton shot, no estimate of the total quantities of contamination in local fallout could be formed. Succeeding shots in this series deposited little contamination on any of the islands.

Just before Shot 5 during Operation Castle, it was found that fallout material remained suspended in the sea. Radiation detectors were hurriedly mounted in aircraft, and the ocean was surveyed following Shots 5 and 6. The work was necessarily limited by the lack of special radiation detectors, sufficient personnel, and aircraft. Because only one aircraft was available, the survey was confined to the area between 20 and 100 miles from ground zero. However, the rough estimates based on this survey data indicate that each of these shots contaminated about 4,000 mi<sup>2</sup> with somewhat less than half of their total fission yield (Reference 3).

The experience during Operation Castle indicated special problems that would arise in aerial surveys, particularly in surveys over the ocean. Navigational correlation would be difficult to achieve over the open sea on long flights. One aircraft could not cover the widespread areas contaminated after megaton-range shots. Isodose data could not be reduced in the aircraft, although required immediately during the flight period to control the aircraft's flight pattern. Barometric altimeters are not accurate enough to provide the close altitude control necessary for relating readings of radiation to an equivalent surface level. And lastly, the radiation detector would need special characteristics for the aerial-survey operations. The detector would need a fast speed of response, shielding to minimize the contribution of aircraft contamination to the readings, and independence from the aircraft supply of power for any critical section of the detector. The voltage from the aircraft generators varies over wide limits, and regulation must be added separately. Also, it would be highly desirable for the detector to have a logarith-



mic response,  $\Box$  that a wide range of radiation intensity  $\Box$  ald be recorded without a change of scales.

The Top Hat aerial radiation detector was developed by HASL to overcome these problems. Units were installed in three AD-5N aircraft and field-tested at the Nevada Test Site (NTS) during Operation Teapot.

The AD-5N aircraft used during Operation Teapot were transferred to an aircraft carrier for surveys following the undersea test during Operation Wigwam (Reference 4). A wide range of radiation intensities were encountered in this operation. The first pass over surface zero was shortly after H + 11 minutes, and measurements were made which extrapolated to approximately 400 r/hr at the surface. At the other extreme, surveys were made at D + 4 days to delineate the edges of the contaminated area, where the dose rates were approximately 0.1 mr/hr.

The Top Hat system was modified for Operation Redwing, and additional units were constructed. No changes were made in the basic detecting elements; however, the hermetic sealing was improved in anticipation of the humidity at the Eniwetok Proving Ground.

#### 1.3 THEORY

The heat resulting from an atomic explosion vaporizes the products of the explosion and the bomb casing. Soil and water in the vicinity of ground zero are also vaporized and picked up by the updraft produced by the rise of the ball of incandescent gases. On cooling, the material in the fireball condenses into particles that include the radioisotopes resulting from the fission process and from neutron activation of inert materials. The energy released in the explosion will influence not only the quantity of particulate material but also its altitude distribution in the vicinity of ground zero. The portion of the yield related to the fission process is represented by the amount of radioactive contamination carried by the particles. Once the particles are formed, they fall and, influenced by the winds, will reach the surface displaced from ground zero. The radioactive fallout from megaton shots may contaminate thousands of square miles of surface.

The shot conditions influence the form and quantity of the fallout. When a shot is exploded on land, a large amount of soil is picked up and much of it is vaporized by the intense heat. This material condenses in a wide range of particle sizes. Some of the radioactive products are condensed around large particles that were picked up in the updraft but not vaporized. These larger particles fall rapidly and reach the surface relatively close to ground zero.

When a shot takes place at the surface of deep water, vaporized water can carry some of the activity away from the site. The large particulate fallout encountered in the land shot will be missing, and this will be reflected in the distribution of fallout on the surface.

An air shot is one in which the fireball does not touch the surface, so that compared with surface shots relatively little foreign material is vaporized. Because there are no available particulates on which the fission products can condense, most of the active material remains in the upper atmosphere and little fallout is likely to be detected in the vicinity of the shot site.

1.3.1 Fallout Contamination of a Water Volume. When the contamination falls into the sea, dispersion and dilution carry much of the material below the surface (Reference 3). The intervening water acts as a shield between the surface and much of the gamma activity. Thus, the radiation dose rates measured above the surface are reduced many orders of magnitude; however, sensitive detectors can be used to delineate the area of contamination. Also, if samples are taken at various depths, the quantity of radioactivity present can be integrated to the maximum depth of mixing, and in this manner, it is possible to secure isodose distributions of the fallout as they would appear on an equivalent land surface.

The location of detector and source volume on a coordinate system is shown in Figure 1.1. Because of the absorption of the gamma rays by the water, radiation detected above the surface comes from the top 10 to 20 cm of the sea. The following equation describes the variation of dose rate,  $I_{\nu}$ , above such a contaminated volume (Appendix A, Equation A.10).

$$= \frac{0.3549}{2} C_{\nu} L(h, \theta) R/hr$$

Where: C = curies per cubic meter

 $I_{\nu}$ 

 $L(h, \theta)$  = a polynomial, dependent on the altitude of the aircraft, h; and half angle,  $\theta$ which subtends the diameter at the surface contamination.

The gamma rays from the fission products are assumed to have an effective gamma energy of 0.5 Mev when 1 to 6 days old (Reference 5). This reference states quantitatively that gamma curies and beta curies are nearly equivalent in this period.

Estimates based on this assumption indicate that contamination with a beta activity of  $4.43 \times 10^{6}$  (dis/min)/liter at the surface should produce a 1 mr/hr gamma flux at 3 feet from the surface, when the diameter of the contamination is large enough to appear infinite ( $\theta$  = 90 deg).



Figure 1.1 Coordinate system of gamma radiation from a water volume.

Fallout of 0.404 megacurie per naut  $mi^2$  deposited in the sea, uniformly mixed to a depth of 60 meters (Reference 3 and Section 3.4.2), would produce a 1 mr/hr gamma field at 3 feet above the surface.

The gamma dose rate at any altitude  $f_a$ , related to the 3-foot value is expressed by the ratio of the polynomials L(h, 90 deg). The altitude absorption  $1/f_a$  is plotted in Figure 1.2.

**1.3.2** Fallout Contamination of a Land Surface. When fallout is deposited on land, the contaminated area appears as a large plane source. At any point in the radiation field, the gamma intensity will include contribution from a circle whose radius is determined by the absorption of the gamma photons in air. The dose rate  $(L_p)$  above such a plane is given by the following equation (Appendix A, Equation A.15).

$$I_p = 3.4427 C_p J(h, \theta) \times R/hr$$

Where: C = curies per square meter

 $J(h, \theta) = a$  polynomial similar in construction to that in Section 1.3.1.

DOE ARCHIVES

(1.1)

With the same assumptions as for the water case (Eo = 0.5 Mev and the ratio of beta and gamma curies equal to 1),  $2.1 \times 10^7 (dis/min)/ft^2$  of beta activity will result in a 1 mr/hr gamma field at 3 feet from the surface, when the source diameter is proportional to  $\theta = 90$  deg. A



10

d.

r

۶r,

gamma fielc 1,000 mr/hr will correspond to a conta ation of 0.356 megacurie per naut mi<sup>2</sup>. The altitude absorption factor, over land, is shown in Figure 1.2.

**1.3.3** Radioactive Decay. Mixed fission products have been assumed to have a radioactive decay proportional to  $t^{-1+2}$  (Reference 6), to reduce the aerial-survey measurements to a common time, t is the time since the detonation.

Large amounts of Np<sup>239</sup> may be found in the fallout from thermonuclear shots. It is possible to calculate the expected increase in the total activity, over that resulting solely from fission



Figure 1.2 Radiation attenuation referred to h = 3 feet.

products, from the capture-to-fission ratio of the device. The decay characteristics of the fallout activity will be modified by the  $Np^{239}$  contribution. The  $Np^{239}$  can be present in amounts up to 50 percent of the total activity, 1 to 3 days after the shot, based on a mixed fission product activity described in Reference 7.

Because of the low energy of the neptunium gamma emission which is predominately 120 kev, the Np<sup>239</sup> adds relatively small contribution to the gamma dose rate when compared to the average fission-product gamma energy. In water the mean free-path length of the lower-energy gamma ray is less than that for the mixed fission product gamma; hence, a lesser volume at the surface of the ocean contributes to the dose rate measured above the surface. This is inversely proportional to the total absorption coefficients of water, at 120 and 500 kev, and reduces the neptunium gamma contribution to 60.6 percent. In addition, the lower-energy gamma flux deposits less energy per unit volume of air, and therefore contributes less to the dose rate. This is an additional reduction to  $18\frac{1}{2}$  percent of the fission product dose rate (Reference 8). The aerial-survey detector response is down to 75 percent at 120 kev energy (Figure 2.5). Because of these factors, even with the neptunium gamma ray contribution to the total activity at 50 percent, the dose rate response in the Top Hat detector will be increased about 4 percent. The relative attenuation, in air, for these two gamma energies, approximately 65 percent, reduces the neptunium gamma contribution to less than  $2\frac{1}{2}$  percent of the fission product dose rate measured at an aircraft ACHIV 300 feet flight altitude.

It is possible that other isotopes may be formed, depending on the type and location of the test. Primary among these is Na<sup>24</sup> produced by neutron activation of the sodium in sea water. This isotope has a 14.8-hour half life and emits two gamma photons, 1.38 and 2.76 Mev. Refer-



ence 6 may be  $\ldots$  d to deduce the dose-rate contribution for an amount, in curies, equal to that for the mixed fission products. The dose-rate measurement at 300 feet is more sensitive to this isotope by a factor of 3.6 because of its increased roentgen conversion from curies, and the larger volume of water contributing to the surface radiation flux.

n

;e

ŝ

<u>y</u>

s,

1.3.4 Distribution of Fallout. To estimate the distribution of fallout, the equation relating gamma dose rate above the surface to contamination density in a volume of sea water may be used in conjunction with the isodose distribution charts and depth of mixing measurements. The contamination density in a thin layer at the surface may be estimated from the average gamma dose rate in the various isodose defined areas. Summation of the estimated contamination would



Figure 1.3 Determination of estimated outer boundary.

yield an estimate of the megacuries of surface radioactivity in the fallout area. This may be correlated with the depth of mixing and the total fallout activity computed.

If the fallout is deposited in the sea, the equation in Section 1.3.1 indicates that a contamination density of 1 megacurie per naut  $mi^2$  would produce a gamma dose rate of 2.5 mr/hr at 3 feet from the surface. The same contamination density, on land, would produce 2,800 mr/hr (Section 1.3.2). For rough estimates, 1 mr/hr at 3 feet over water is equivalent to a 1,000:1 increase in activity per naut  $mi^2$  when compared to 1 mr/hr on land.

The calculations for land and water are summarized as follows: on land, 1 mr/hr at 3 feet is equivalent to  $2.1 \times 10^7 (dis/min)/ft^2$  or  $3.56 \times 10^{-4}$  megacuries/naut mi<sup>2</sup>; on water, 1 mr/hr at 3 feet is equivalent to  $4.43 \times 10^6 (dis/min)/liter$  or  $4.04 \times 10^{-1}$  megacuries/naut mi<sup>2</sup> where depth of mixing is 60 meters.

When the fission product falls into the sea, the outer boundary of the contaminated area will be indicated by gamma-radiation readings that are only slightly above the background gamma dose rate. Figure 1.3 illustrates the radiation profile across a contaminated area. The estimated outer boundary (EOB) from a shot with a high-fission yield is indicated at A and D. A shot with the same total energy yield, but producing a smaller quantity of fission products, will have an EOB at B and C. Both shots may have the same actual outer boundary, yet the minimum detectable limit of radiation of the instrumentation will result in a low estimate for the area. For material-balance calculations, the quantity of radioactivity outside the EOB will be small in relation to the quantity located in the higher-intensity areas.



## Chapter 2 PROCEDURE

#### 2.1 SHOT PARTICIPATION

Prior to the operation, aerial surveys were scheduled to follow Shots Cherokee, Zuni, Flathead, Navajo, Apache (secondary participation), and Tewa. Because Shot Cherokee was delayed, Program 2 requested that the project add Shot Lacrosse to its schedule in order to give the aerial survey an opportunity to obtain operational experience. However, this survey was cancelled, because flight clearance below 1,000 feet in the region of Eniwetok Atoll could not be obtained.

A change in the Apache scheduling introduced a conflict with the project's participation during Navajo. The new schedule called for dual capability involving both Eniwetok and Bikini Atolls. Participation in Apache was therefore, canceled.

Because of the long waiting period between Flathead and Navajo, the project requested secondary participation in Shot Mohawk.

Preshot surveys were flown before the Navajo and Tewa shots, based on a Program 2 request, to define the background status resulting from the flow of contaminated lagoon water over the reef at Bikini.

Helicopter missions, for altitude absorption data, were originally scheduled after Shots Seminole, Mohawk, and Navajo. The mission for the latter was subsequently canceled at the request of the project, because of a shortage of personnel. During June and July, it was necessary to assign two technicians to Kwajelein to service the aerial-survey equipment; therefore, they were no longer available for on-site operations.

The project operations are summarized in Table 2.1.

#### 2.2 OPERATIONS

Many projects in Program 2 studied different phases of fallout. Project 2.64 developed isodose plots of the contaminated area by aerial surveys. The operations were primarily to secure aerial survey data; subsidiary measurements were performed in support of this objective to correlate this data. Altitude absorption studies were required to verify the correction factors used in relating the aerial survey to a reference plane 3 feet above the surface.

#### DOE ARCHIVI

2.2.1 Aerial Surveys. Four P2V-5 aircraft were assigned for the project operations, and were administratively attached to the Security Squadron, Patrol Squadron 1. Three of the aircraft were supplied from outside the squadron, and the fourth came from its assigned strength. The squadron provided all maintenance and operational control. This control was shifted to the Program 2 Control Center on the USS Estes, AGC-12, during the aerial-survey flights. The Air Operations Officer, Task Group 7.3, assumed primary radio guard during this period.

The plan of the project air control in the Program 2 Control Center is shown in Figure 2.1. The communication routing is shown in Figure 2.2. The telemeter operator logged all incoming radiation readings, which were immediately recorded on a time-based continuous plot. Navigational information was received from the radio operator on Channel C (6693 kc). The Project 2.64 Operations Officer correlated the navigational and radiation data on the rough flight-control chart. The plotter transferred this information to the tactical isodose plot, under the supervision of the 2.64 Project Officer, who used the flight and isodose charts to determine the next area of search for each aircraft. The operations officer laid out the required navigational ref-



erences for the  $\Rightarrow$  ignated flight legs and transferred this  $\Rightarrow$  rmation to the working flight log. The Task Group 1.3 Air Operations Officer reviewed the legs for flight safety, and the information was relayed to the appropriate aircraft by the radio operator.

D-day flights used one aircraft, with a second aircraft on standby. The flights were limited to the upwind areas until active fallout had ceased. Surface ship reports, received by the Proj-

Shot	Date	Time	Location	Aerial Survey	Altitude Absorption
Cherokee	21 May	0551M	Bikini	D-day D+1	
Zuni	28 May	0566M	Bikini	D-day D+1 D+2 D+3	
Seminole	6 June	1255M	Eniwetok		D-day
Flathead	12 June	0626M	Bikini	D-day D+1 D+2	
Mohawk	3 July	0606M	Eniwetok	D+1	D+2
Navajo	11 July	0556M	Bikini	D-3* D-2* D-day D+1 D+2 D+3	
Tewa	21 July	0546M	Bikini	D-1* D-day D+1 D+2 D+3 D+4	

TABLE 2.1 SUMMARY OF PROJECT OPERATIONS

l

\* Preshot surveys of lagoon water outside the Bikini Atoll.

ect 2.63 representatives in the Control Center, indicated when fallout had stopped in the close-in downwind sector. The aircraft was then controlled through the area to limits described by the ship reports. The D-day flights delineated the upwind boundary and obtained some intensity readings in the radioactive area immediately downwind of ground zero.

Two aircraft were used on D + 1. One delineated the close-in radioactive area and confirmed the upwind boundary located on the previous day. The second aircraft flew an extensive search pattern to locate the edges of the contaminated area.

The D + 2 survey re-examined the overall contaminated area. One aircraft was usually sufficient. However, the Tewa pattern was so large that two aircraft were needed. Flights on subsequent days used one aircraft and tracked the area until the dose rates became too low for adequate delineation.

Survey data which delineated the outer boundary and points of interest in the fallout pattern were plotted in the control center to guide the Project 2.62 surface ships with their oceanographic surveys.

During the period prior to the next shot, each aircraft was scheduled to spend a day on Site Fred for instrument calibration and service. Two technicians calibrated each radiation detector at Kwajalein prior to and immediately following each survey flight and returned the Top Hat detectors to Site Elmer between shots, where a complete routine battery change and recalibration was performed.





Figure 2.2 Communication routing, Project 2.64 air control.

2.2.2 Altitu Absorption. Because considerations of it safety limit the minimum altitude at which aircrait can fly over water, automatic gamma monitors were mounted over the sides of two ships of Project 2.10, to measure the gamma-radiation field at 35 feet above the sea surface. This was to provide low-altitude readings simultaneous with aircraft passes in the same area at higher altitudes.

Survey aircraft made altitude-calibration passes over islands of the Eniwetok Atoll after Shot Mohawk. After Shot Tewa, the P2V-5 dropped a smoke light in the open sea to be used as a navigational reference and made altitude passes in the vicinity. These data are examined for the variation of radiation reading between different flight altitudes and given in Section 3.2.

Helicopter missions, after Shots Seminole and Mohawk, obtained data similar to the altitudecorrection-calibration data collected by the survey aircraft. Because the helicopters could not safely hover at low altitudes, complete information could not be obtained. It had been planned to obtain gamma-energy spectra at various altitudes above a contaminated surface. The Top Hat dose-rate response was to be compared to the gamma-energy spectra to determine whether the assumption of air-equipment response was valid. However, instrumentation difficulties and the limitations in hovering altitudes resulted in fragmentary data. The survey using a scintameter obtained dose-rate readings at altitudes between 25 and 1,000 feet.

#### 2.3 INSTRUMENTATION

The major instrumentation consisted of aerial radiation detectors. Scintillation survey meters and ship-mounted gamma monitors were used for measurements relating to altitude-correction factors. A spectrometer was used to obtain the distribution of the gamma energies at survey altitudes. The instruments are described in Appendix B.

2.3.1 Aerial Survey. Each of the project aircraft had the following equipment: (1) Top Hat aerial radiation detector, HASL TH-10-B (Appendix B); (2) detector control assembly, HASL TC-14-A; (3) strip-chart recorder, Esterline Angus Co., AW; (4) telemeter assembly, HASL TT-3-X; (5) power supply, HASL TB-6-A; and (6) radio transmitter, U.S. Navy ART-13. The permanent components were installed by the Overhaul and Repair Department, U.S. Naval Air Station, Alameda, California, at the air station prior to Operation Redwing. The removable components were installed by project personnel after the squadron deployed to the EPG.

The location of the assemblies is indicated in Figure 2.3. The radiation detector was mounted aft to avoid the major areas of aircraft contamination, namely, the engines, oil-cooler air intakes, leading edges of the wings, propellers, and front of the radome. The cabin intake vents were sealed to prevent contamination of the interior ductwork. The control assembly and the operator were placed forward, next to the navigator. This facilitated close correlation between the navigational and radiation reports. The remainder of the equipment was located on an available-space basis.

The relationship of the various sections, both in the aircraft and in the Program 2 Control Center, is shown in Figure 2.4. The radiation detector and its associated control assembly drives a strip-chart recorder to provide a permanent, continuous record of the radiation intensities as measured in the aircraft. This detector is nearly air-equivalent from 30 to 1,400 key. Figure 2.5. An annular radiation shield is built into the detector to reduce the effect of aircraft contamination. The angular response due to this shield is shown in Figure 2.6.

The aircraft's radio altimeter (U.S. Navy APN-1) supplies an altitude indication to the altitude compensator, which modifies the radiation detector so that its output is a current that is proportional to the radiation which would be measured at 3 feet above the surface. As the altitude changes, the compensator corrects the resulting radiation change and keeps the ground-level reading constant.

The telemetering system did not perform satisfactorily. The radiation readings on the **aircraft radiation**-detector strip-chart recorder were, therefore, transmitted by voice over the **navigational net**. At the control center, the radiation readings were logged and immediately **plotted**.

2.3.2 Altitu. Absorption. The automatic gamma mon. s, HASL TN-4-C, were mounted on the YAG-39 and YAG-40. Each instrument was mounted at the end of a boom that was also used to suspend the depth probe of Project 2.62. The boom extended 35 feet from the side of the ship and was set at an approximate mean height of 35 feet above the sea. An Esterline-Angus strip-chart recorder was installed in the shielded control room on the ship, to continuously record the gamma dose rate. The installation of the monitors and recorders was accomplished by Project 2.10.

Scintameter survey meters, HASL TH-3-B and TH-7-A, were used for helicopter operations. Gamma dose rate was measured at various altitudes over contaminated water and land surfaces.



Figure 2.3 Radiation-survey-equipment mounting locations in P2V-5 aircraft.

A gamma spectrometer, HASL TM-10-A, which consists of a scintillation head, pulseheight-analyzer, and a recorder, was loaded into the same helicopter. The 28-volt power in the helicopter was converted to 115 volts, 60 cps, by a separate inverter to supply the spectrometer. The count rate at various energy levels was observed on a meter as the base line automatically swept through an energy scan from 50 kev to 3 Mev.

The survey aircraft had the same instrumentation as described in the previous section, plus a scintameter survey meter, TH-3-B.

DOE ARCHIVES

17

-----

#### 2.4 REQUIRED DATA

The project operations were directed mainly toward obtaining isodose plots of the gamma







DOE ARCHIVES

21

\* **57**°, 13



Figure 2.5 Energy dependence of dose rate response, Top Hat plastic phosphor,  $1^1\!/_8-$  inch diameter by  $^3\!/_8$  inch long.



Figure 2.6 Angular response of Top Hat radiation detector; DCE ARCHIVES measured with 1-mg radium source.



dose rates resulting from fallout in the sea. Only those sub-idiary measurements which were directly applicated to an understanding of the aerial-surve technique were undertaken.

2.4.1 Distribution of Contamination in the Sea. The gamma isodose plots may be directly related to the surface layer of contamination in the sea. To obtain these plots, gamma dose rate was recorded in the aircraft as it was flown on a search pattern. The aircraft flew between designated points at constant speed. The plot of the flight leg was then marked with time divisions. The recorder chart is calibrated in time, so the gamma reading can be related to the position of the aircraft. Readings were plotted on the flight chart, and points of equal dose rate connected to develop the isodose chart. The values of these isodoses were then corrected to H + 24 hours and to 3 feet above the surface.

2.4.2 Altitude Absorption. To refer the aircraft readings to 3 feet above the surface, verification of the attenuation resulting from air absorption was required. Survey aircraft and helicopter passes at varying altitudes were made over fixed locations to obtain the gamma dose rate as a function of altitude.

2.4.3 Stability of Contaminated Area. Variations in the density of surface contamination during an aerial survey can modify the estimates of the location on an isodose line, because various points along this isodose must necessarily be determined at different times. The surface stability is directly influenced both by surface ocean currents that horizontally translate the contamination, and by mixing which removes contamination from the surface. The gamma-intensity measurements made by aerial surveys cannot view the gamma activity of contaminated area may be achieved by comparing the aerial-survey results over a period of several days. The change in position of the isodose lines provides information on the horizontal translation of the surface contamination.

Data on the vertical-mixing function may be obtained directly by the analysis of samples taken from varied depths at a specific location. The analysis is included as Appendix D.

### DOE ARCHIVES



## Chapter 3 RESULTS

#### 3.1 INSTRUMENTATION PERFORMANCE

The bulk of the radiation-detection equipment performed satisfactorily throughout the operation. The limit of detectability was determined by the background dose rate on, or close to, the detector. Because the source of radiation to be measured, namely the surface of the sea, was located considerable distance from the radiation detectors, contamination on or close to the detector units would contribute a relatively large portion of the total reading.

The aerial-survey dose-rate measurements were continuously recorded and stored on a stripchart recorder. The strip charts were correlated with the navigational logs to develop preliminary isodose plots. The results of the surveys are presented in this compiled form. The altitude absorption measurements are presented as gamma dose rate versus altitude and have been fitted to an appropriate, derived curve.

3.1.1 Aerial Surveys. The records of 37 pre- and post-flight calibrations of the Top Hat detectors have been summarized in Figure 3.1. Thirty-two calibrations were within plus or minus 1 percent of the desired curve. This is within the reading accuracy of the recorder. A 1-percent instrument stability corresponds to a 10-percent radiation variation because of the logarithmic character of the scale. All calibrations were within a maximum limit of  $\pm$  25 percent of the desired response.

As mentioned previously, the automatic telemetering system failed to provide reliable transmission of the aircraft data to the control center on the USS Estes, AGC-12. Voice relay of the recorder readings over the navigational net, Channel C, was substituted. The ship's radio receivers did not provide clear, long-range communication with aircraft operating at an altitude of 300 feet. A radio receiver, U.S. Army R-390, was obtained from Task Unit 3 and tuned to the aircraft frequency, Channel C. The R-390 had a lower noise level, and the aircraft transmissions could be clearly detected at a greater distance. When an aircraft exceeded the reliablecommunication range, messages were relayed through a second aircraft.

3.1.2 Altitude Absorption. The automatic gamma monitors mounted on the YAG-39 and YAG-40 were calibrated for each shot participation prior to departure from Site Elmer. Examination of the calibration records shows close conformity to the desired radiation response.

A plastic bag was used to protect each monitor. However, the bag became contaminated during fallout, and the readings of sea activity were completely masked. The readings could not be used to provide a surface measurement for aircraft-altitude calibration.

The scintameter survey meter was calibrated just prior to each helicopter mission. Longterm stability was not required for this application.

When used in a helicopter, the gamma spectrometer required alternating current power which was supplied by inverters fed from the 28-volt supply in the helicopter. During Shot Seminole, the vibrator-type inverters failed. Rotary converters were obtained, and a dry run scheduled prior to Shot Mohawk. The energy response was checked against sources containing known radioisotopes, and the performance was satisfactory. The mission was flown on Mohawk D + 2. On arrival at the station, the recorder failed because of the heavy vibration encountered during the hovering of the helicopter. Visual observation of the meter was used to obtain general energy distributions at 500 and 800 feet. The pilot was unwilling to risk hovering at lower altitudes.

24

DOE ARCHIVES



#### 3.2 ALTITUDE ABSORPTION MEASUREMENTS

Data on radiation versus altitude, over land, are summarized in Table 3.1. Scintameter survey meters were used for the measurements during helicopter missions. A Top Hat radiation detector and a scintameter were used in the P2V-5 aircraft.

The differences in the absolute values of the readings in the P2V-5 are due to the difference





in the energy response of the two types of detectors. The scintameter, TH-3, uses a sodium iodide phosphor, which is more sensitive to soft gamma radiation. The Top Hat detector uses a plastic phosphor and has a response that is nearly energy-independent. The response of the two types of instruments is summarized in Figure B.2. Because fresh fission products have a

25



DOE ARCHIVES

#### TABLE 3.1 ALTITUDE RADIATION DATA OVER LAND (ENIWETOK ATOLL)

ltitude	mr/hr•	mr/hr†	mr/hr‡	mr/hr§	mr/hr¶	mr/hr**
ft						
1,000				1.0, 1.1†	t	
800			130	1.5		
600			180	1.8		
500	0.7				18	5.7
400				2.8		
300	1.0	1.2			30	8.5
200	1.9	1.9	500	4.1	42	12.5
100			950		70, 55††	18.0
75			1,200			
50	2.5	2.3	1,700	11.0		

\* Mohawk + 2, over Tilda, scintameter TH-3, S/N 25 in helicopter.

 $\dagger$  Mohawk + 2, over Tilda, scintameter, TH-3, S/N 2 in helicopter.

1 Mohawk + 2, over Sally, scintameter, TH-7, S/N 3 in helicopter.

§ Seminole D-day, over Janet, scintameter TH-3 in helicopter.

¶ Mohawk + 1, over Janet, scintameter, TH-3, in P2V-5.

\*\* Mohawk + 1, over Janet, Top Hat radiation detector in P2V-5.

tt Values from repeat runs.

gamma-emission energy that is considerably softer than the radium used in instrument calibration, the sodium iodide detector should read high on an actual survey.

The data in Table 3.1 were normalized to the theoretical curve, and are shown in Figures 3.2 and 3.3. م م م



Figure 3.2 Radiation attenuation over land (Helicopter).

Table 3.2 summarized the data obtained over water, and these are plotted in Figure 3.4. Additional data of this type have been derived from measurements made in previous operations. This information is presented in Appendix C. The curves in Figures C.1 and C.2 show a similar correspondence to the theoretical curves.



Figure 3.3 Radiation attenuation over land (P2V-5 aircraft).



Figure 3.4 Radiation attenuation over water.

27

24

÷

As discussed in Section 3.1.2, the distribution of gamma energies was estimated from the visual observations of a meter on the gamma spectrometer. Observations at 500 and 800 feet above Site Sally on Mohawk D + 2 showed a general response where the predominant portion of the energy spectrum fell between 350 and 600 kev.

#### 3.3 DISTRIBUTION OF FALLOUT

The isodose charts contained in this section have been referred to H + 24 hours and gamma dose rate at 3 feet above the surface. The decay correction is based on  $t^{-1.2}$ . The flight altitude was 300 feet for all surveys, so the altitude correction is based on a factor of 2.5.



Figure 3.5 Flight pattern, Shot Cherokee D-day.

The EOB is based on a minimum detectable limit by the detector of 0.01 mr/hr. This converts to 0.025 mr/hr at the surface. Where there are no flight legs in a position to close an isodose plot, dotted lines indicate the estimated position. The estimates are based on previous days' results wherever possible. Contamination enclosed within an isodose bounded area is calculated on the basis of the average gamma intensity between consecutive isodose lines, and a contamination density of 0.4 megacurie/naut mi<sup>2</sup> for 1 mr/hr of gamma dose rate (Section 1.3.1).

DOE ARCHIV

**3.3.1** Shot Cherokee. The D-day flight encountered no radiation intensities above the detectable limit. The flight pattern is included to show the area searched (Figure 3.5). The D + 1 flight was used for instrument check, because no contamination was found on the previous day.

3.3.2 Shot Zuni. The D-day flight examined the region in the vicinity of the atoll (Figure 3.6). Because there was not enough data to develop isodose plots, radiation profiles have been plotted along the flight legs.





....

S



The D + 1 fli  $\rightarrow$  located the EOB and delineated the co. ..., inated areas (Figure 3.7). A contaminated patch was suspected to be northeast of Bikini, based on the control center plots. During the data reduction, a navigational reporting error was discovered which changed the relatively isolated patch from the northeast to a position almost due east of Bikini.

Altitude	mr/hr*	mr/hr†	mr/hr‡
ft			
1,000			0.41
800			0.52
700	0.12	0.225	
600	0.135	0.225	1.1
500	0.135	0.29	
400	0.175	0.38	2.1
300	0.175	0.42	
200	0.225	0.62	1.4, 1.7\$
50			2.6, 3.0§

#### TABLE 3.2 ALTITUDE RADIATION DATA OVER WATER

\* Tewa + 3, 12-01 N, 164-41 E, Top Hat detector in P2V-5.

† Tewa + 3, 12-11 N, 165-02 E, Top Hat detector in P2V-5.

\$ Seminole D-day, off Janet, scintameter, TH-3,

in helicopter.

§ Values from repeat runs.

The D + 2 flights (Figure 3.8) investigated the northeast sector without discovering contamination. The eastern contamination was not suspected until the data-reduction period, so no further examination was scheduled in that sector.

The D + 3 flights (Figure 3.9) reconfirmed the hot area. No further flights were scheduled,

Isodose	Area	Difference Area	Average	Conta	amination
mr/hr	mi²	mi <sup>2</sup>	mr/hr		mc
D+1					
1.25	165	165	1.25	83	
0.25	4,677	4,512	0.59	1,065	
0.125	8,433	3,756	0.18	270	
0.025	13,683	5,250	0.06	126	
				1,544 r	mc at H+24 hou
D + 3					
0.75	757	757	1.25	379	
0.25	6,775	6,018	0.50	1,204	

TABLE 3.3 SUMMARY OF FALLOUT DISTRIBUTION, ZUNI

as low intensities were encountered on this day.

The fallout distribution is summarized in Table 3.3.

3.3.3 Shot Flathead. The D-day flight discovered relatively high dose rate just west of Bikini (Figure 3.10). The position immediately adjacent to the reef indicated that this could be lagoon water passing over the reef, rather than fallout. This area was not completely mixed,









as the D + 1 sugged became contaminated. A replacement aircraft was flown to the survey area. This also became contaminated. At no time was the level in the aircraft allowed to exceed 20 mr/hr.

Both aircraft on the D + 1 flights (Figure 3.11) were also lightly contaminated. Active fallout was encountered 100 miles northwest of Bikini at H + 30 hours. The northwest sector was closed, as far as aerial surveys on D + 1 were concerned. As indicated on the chart, it was not possible to close the isodose plot at that time.

The project had four aircraft to choose from for the D + 2 flight, all reading a background of approximately 0.1 mr/hr inside the detector shielding. The survey for this day could not detect any surface contamination reading above a minimum detectable limit of 0.25 mr/hr at 3 feet from the surface. Table 3.4 summarizes the fallout distribution.

Isodose	Area	Difference Area	Average	Contamination
mr/hr	mi <sup>2</sup>	mi <sup>2</sup>	mr/hr	mc
D+1				
0.2	383	383	0.368	56
0.1	908	525	0.148	31
0.05	3,350	2,442	0.074	73
0.025	11,000*	7,650*	0.037	115
				275 mc at H+24 hours

TABLE 3.4 SUMMARY OF FALLOUT DISTRIBUTION, FLATHEAD

\* Based on estimated position of isodose line.

The EOB is roughly estimated and may not be representative of the actual extent of the contamination.

**3.3.4** Shot Mohawk. A survey of the islands of Eniwetok Atoll was flown on D+1. The island readings are shown in Figure 3.12. The readings are referred to 3 feet above the surface of the islands by a factor of 5.8 for the 300-foot flight altitude (Figure 1.2). Sites Fred and Elmer were excluded from the survey pattern, because a 300-foot flight altitude would have interfered with the air traffic in the vicinity. The open-sea aerial survey could find no detectable contamination in the area searched (Figure 3.13).

**3.3.5** Shot Navajo. A background survey was made on D-1 day to determine if the hot intensities, reported by Project 2.62, adjacent to the reef after Shot Flathead, could have come from contaminated water crossing the reef. This flight (Figure 3.14) subsequently became a D-3 survey because of postponement of the shot. The next flight (Figure 3.15) became the D-2 survey, again because of a postponement. The aircraft flight, on the day which would have resulted in a D-1 survey, was not completed because of malfunction.

The background surveys were coordinated with a Project 2.62 ship survey. Because the shape and position of the contaminated area varied from day to day, it is possible that the variation may have been a function of the surface winds. An outline of the area, based on the ship data has been included as Figure 3.16. The agreement between these plots appears good, in view of the 12-hour displacement between the ship and aerial survey.

The D-day survey (Figure 3.17) located the estimated upwind boundary. On D+1, the flights covered an area of 10,000 mi<sup>2</sup> but did not close the 0.025 mr/hr isodose line in the northwest sector (Figure 3.18). The D+2 chart (Figure 3.19) shows that this isodose extended farther than estimated on the previous days. The narrow 1.25 mr/hr line extending to the west of the ARCHIVE atoll had disappeared. Reef readings have been included in this chart.

The summary of the fallout distribution (Table 3.5) indicates considerable instability in the contaminated area during the aerial-survey operations. As experienced after the previous water









**DOE** ARCHIVES

Figure 3.12 Atoll readings, Shot Mohawk, D+1 day. All readings referred to mr/hr at 3 feet from the surface and to the time of the survey. Sites Elmer and Fred not surveyed.





Figure 3.13 Flight pattern, Shot Mohawk, D+1 day.










TINN VILLA I TIN VINGLI

.



shot, Flathead,  $n_{-}$  th of the fallout remains airborne. Thus, allout and mixing in the sea could be expected to persist well into D+1.

**3.3.6** Shot Tewa. A D-1 survey (Figure 3.20) defined the background status to the west of the atoll, prior to the shot. The D-day flight (Figure 3.21) located the upwind boundary. The

Isodose	Area	Difference Area	Average	Contamination
mr/hr	mi²	mi <sup>2</sup>	mr/hr	mc
D + 1				
1.25	158	158	1.35	85
0.25	958	800	0.75	240
0.125	1,788	830	0.18	60
0.025	10,490*	8,702	0.06	209
				594 mc at H+24 hours
D+2				
1.25	90	90	1.35	49
0.25	1,267	1,177	0.75	353
0.125	3,263	1,996	0.18	144
0.025	20,930*	17,667	0.06	424
				970 me at H+24 hours

TABLE 3.5 SUMMARY OF FALLOUT DISTRIBUTION, NAVAJO

\* Based on estimate of isodose position.

D + 1 survey (Figure 3.22) discovered a contaminated area extending over 200 miles west of Bikini. The outside boundary could not be closed on this survey, because of the far-out sector contained active fallout from Shot Huron. The D+2 survey (Figure 3.23) extended the estimated position of the EOB. The isodose was still not completely closed. The aircraft was not allowed to lose radio contact, so the survey covered only the area out to 275 miles from Bikini.

The 0.25 mr/hr isodose extended into the far northwest sector on D+1. By D+2, the position had shrunk to approximately a third of the enclosed area. The predicted pattern shows that this far-out material could not be expected to arrive before H+19 hours. Thus, it is probable that the readings in the area on D+1 were due to material that was not completely mixed. By D+2, some 30 hours had elapsed, and mixing was probably complete.

The D+3 and D+4 surveys, Figures 3.24 and 3.25, delineated the hot area, permitting an examination of the shape and position of these inner areas from D+1 through D+4. Table 3.6 summarizes the fallout areas throughout the shot participation.

#### 3.4 SAMPLES OF CONTAMINATED SEA WATER

Duplicate samples of sea water were furnished to this project by the U.S. Naval Radiological Defense Laboratory (NRDL) and by Scripps Institution of Oceanography (SIO) from their seasampling programs. After the close of Operation Redwing, these samples were analyzed for beta activity in the particulate and salt fractions at the HASL.

### DOE ARCHIVE

**3.4.1** Gamma Radiation as a Function of Beta Activity. The analysis of each sample, the gamma intensity estimated at each sampling location, and the comparison of these results are contained in Appendix D. A straight averaging of the beta activity and the estimated gamma intensity yields a figure of  $4 \times 10^6$  (dis/min)/liter per mr/hr. The wide variability of the comparison for each sample obviates definite conclusions. However, much of the data falls within  $\pm 50$  percent of the theoretical calculation of  $4.43 \times 10^6$  (dis/min)/liter of beta activity per mr/hr of gamma activity 3 feet above the surface. Thus, these results may be considered indicative of validity of the assumption.



Figure 3.19 Flight pattern, with a Numbers show legs 110w11 with the 24 hours and 3 feet above surface.









----

**.**99 H+24 hours and 3 feet above surface. Numbers show legs flown by Aircraft 1; Figure 3.23 Flight pattern, Shot Tewa, P+2 days. All data readings refer to 165 164 letters show legs flown by Aircraft 2. 163 162 .i9 DOEARCHIVES ē

---- Estimated Location of Isodose Lines

8

Noutical Miles

49





t-



Isodose	Area	Difference Area	Average	Contamination
mr/hr	mi <sup>2</sup>	mi <sup>2</sup>	mr/hr	mc
D+1				
2.5	1,230	1,230	5	2,460
1.25	2,390	1,160	1.84	858
D + 2				
2.5	1,150	1,150	5	2,300
1.25	2,340	1,190	1.84	880
0.25	6,750	4,410	0.75	1,323
0.025	43,505	39,095	0.125	1,955
				6,458 mc at H+24 hours
D+3				
2.5	982	982	5	1,964
1.25	2,035	1,053	1.84	779
D+4				
2.5	1,070	1,070	5	2,140
1.25	1,695	625	1.84	462
0.25	3,580	2,955	0.75	88 <b>7</b>

### TABLE 3.6 SUMMARY OF FALLOUT DISTRIBUTION, TEWA

TABLE 3.7SUMMARY OF DEPTH SAMPLES OF SEA WATER

THE REAL PROPERTY OF THE PROPERTY OF THE REAL PROPE

Shot	Station	Sample Time	Distance*	Surface	Total
		H+hours	naut mi	10 <sup>3</sup> (dis/min)/liter	$10^{3}(dis/min)/cm^{2}$
Flathead	F-2	29.5	32	20	93
Flathead	F-5	49.5	39	32	205
Navajo	N-17	90		230	658
Tewa	T-5	41	31	266	1,514
Tewa	T-7	52	- 54	124	563
Tewa	T-8	59	13	51	412

\* Distance from surface zero.

DOE ARCHIVES

ande stade ne





باللاله والمعارة اللهابي بعاد ومركبك

100

50

-----

**3.4.2** Depth of Mixing. The analyses of samples from various depths are included in Appendix D. The summary of these results (Table 3.7) show beta activity of the surface samples, and the integrated area under the curve for depth versus beta activity of sample. This area is representative of the total activity contained under a square centimeter of ocean surface.

.

The surface and total activity are plotted in Figure 3.26. This figure indicates an effective depth of mixing of 60 meters for fallout deposited in the sea around Bikini Atoll. A more thorough discussion of the mixing function may be found in Reference 9.

54

### DOE ARCHIVES

## Chapter 4 DISCUSSION

The accuracy of the dose-rate measurements depends on the navigation, instrumentation, and correction factors that refer the aircraft readings to the 3-foot references plane. The isodose plots most closely represent the actual fallout distribution in the region where the flight legs are close together. Less information is available in the far-out areas, because of the greater distances between the legs of the flight patterns. The position of isodose lines are estimated between the measured equal dose-rate points.

### 4.1 OPERATIONAL PERFORMANCE

The records of the Top Hat aerial survey meters indicate that their calibrations remained stable throughout the surveys. Complete and frequent calibrations were made to insure optimum operation of the equipment. Only one breakdown, an interconnecting cable break on Zuni D-day, occurred during the entire operation.

The failure of the automatic telemetering link between the aircraft and the control center created the requirement for more intensive clerical effort in the data-collection period. Voice transmission of the data provided immediate information for the tactical isodose plot and the flight-control chart, but the aircraft positions and radiation records had to be reviewed during the development of the survey plots.

The airborne radioactivity encountered after Shot Flathead limited the contaminated-area survey. The EOB of the fallout could not be detected after the aircraft became contaminated; however, high-value isodose data were obtained, and a partial plot was developed.

#### 4.2 DATA RELIABILITY

Errors in delineation of areas enclosed by isodose lines depend on variations during the survey and on the estimates of isodose positions between measured points. Navigational accuracy, variations in the individual radiation detectors, and the accuracy of determining the aircraft altitude contribute to the accuracy of the primary measurements.

Determinations of surface dose rate and contamination are dependent on the primary measurements and the accuracy of the theoretical calculations.

**4.2.1** Isodose Determinations. Navigation was based on Loran fixes at the end, and at points during each flight leg. Each transit along a flight leg was flown at constant speed and course heading. The aircraft positions are estimated to be within a 3-mile error circle at any time.

The radiation response of the Top Hat detectors was assumed to be represented by the calibration curve (Figure 3.1). Reproducibility of all instruments was within 10 percent for over 87 percent of the calibrations, and no instrument exceeded 25 percent at any time. The change in radiation intensity at the edges of the highly contaminated sections is rapid. A 20-percent error in the reading will not displace the 0.25 to 1 mr/hr isodose contour by over a mile. This is well within navigational accuracy.

The aircraft are assumed to have been within 5 percent of their reported altitude, based on the HIVES specified accuracy of the APN-1 radio altimeter. This altimeter indicates the altitude between surface and aircraft directly and is not dependent on atmospheric pressure. Altimeter error does not appear directly in the results, rather the error is modified by the slope of the altitude





correction factor. The altitude error at the 300-foot level has a maximum value of 15 feet based on the APN-1 specification. The altitude correction-factor error will be less than 4 percent.

The absolute value assigned to an isodose depends on the calibration of the radiation detector and altimeter, and on the altitude-correction factor. The major assumption of an average gamma-emission energy of 500 kev in evaluating the altitude absorption derivation is supported by the gamma-spectrometer results (Section 3.1.2), and the ratio of the radiation readings of an energy-dependent detector and the Top Hat detector during a survey over the Eniwetok Atoll (Section 3.2).

**Examination** of the radiation dose-rate relations between various altitudes over land and water **during Operation** Redwing (Section 3.2), during previous operations (Appendix C), and during Operation Plumbbob (Reference 12) indicate the validity of the assumptions and the accuracy of the **calculated altitude**-correction values.

4.2.2 Contamination-Density Determinations. As indicated in Section 1.3.4, fallout on a land surface is expected to produce, at 3 feet from the surface, a gamma dose rate about 1,100 times higher than the dose rate resulting from the same fallout density in the sea. Agreement of data with the theoretical derivation primarily depends on the accuracy of three factors: (1) the depth of vertical mixing, because material below the surface of the sea will not contribute to the gamma field, (2) the average gamma-emission energy, which determines the thickness of the surface layer that does contribute to the gamma field, and (3) the air absorption, which determines the surface area viewed by the radiation detector. The equivalent depth of mixing was estimated as 60 meters (Section 3.4.2). This is in essential agreement with measurements made during Operation Castle.

The experimental work was based on only a few stations and did not necessarily represent the conditions throughout the fallout area. However, variation in mixing will introduce ariations in the area enclosed by an isodose contour; this is discussed in Section 4.3.1. The average gamma energy and the altitude absorption characteristics assumptions are supported by several measurements as discussed in Section 4.2.1.

There is one direct comparison of the land and water equivalence based on the fallout following Tewa (Figure 3.23). The isodose pattern encloses Parry Island, Eniwetok Atoll. This island is located between the 25 and 250 mr/hr land-equivalent isodose lines (0.025 and 0.25 mr/hr water isodose). Radsafe measurements indicate a gamma dose rate between 100 and 125 mr/hr on Parry at 24 hours following Shot Tewa.

The contamination density calculations are based on the factors discussed above, and on the relationship between beta and gamma curies. A direct comparison of the conversion between gamma dose rate and beta specific activity is discussed in Appendix D. The measurements are not conclusive. However, the general trend of this data does agree with the theoretical calculations (Section 1.3.1).

### 4.3 DISTRIBUTION OF CONTAMINATION IN THE SEA

The fallout estimates based on the aerial-survey charts show a definite relation to the fission yield. However, the distribution of this material is not related to the total energy yield, because the conditions of the shot—water, land, or air—affect the fallout. Meteorological conditions also play a major part in determining the area of contamination.

**4.3.1** Stability of Contaminated Area. Fallout deposited in the sea is acted upon by the ocean currents, producing a horizontal translation of the location of the material, and a vertical displacement based on the mixing of the material in the sea volume. To obtain a measure of the stability over a period covered by the aerial surveys, measurements were repeated from day to day. All gamma radiation measurements were referred to 3 feet from the surface and to H + 24 hours so that a common comparison could be made for any particular isodose area. The horizontal translation is clearly indicated by the positional shift of the isodose pattern. The vertical mixing is indicated by the amount of area enclosed within the described pattern.

The mixing of -radioactive material in the ocean will --rease the amount of gamma fluxwhich may be measured in the aircraft. If the survey is made soon after fallout ceases, thismixing will not be complete. On D+1, Shot Tewa, the 0.25 mr/hr contour extended nearly 200miles west and northwest of Bikini. The survey on D+2 placed the end of this isodose patterncloser to ground zero. The aerial flight surveyed the fallout area approximately 6 hours afterthe fallout, and mixing was apparently not completely uniform to the thermocline. By the nextday some 30 hours had elapsed, much of the material had been removed from the surface, andit is expected that the mixing was more nearly uniform, as represented by the data described inAppendix D.

The area enclosed by a particular contour appears to be stable for a relatively long period of time. The 2.5 mr/hr isodose after Shot Tewa was followed for several days. While the effect

TABLE 4.1 FALLOUT SUMMARY

ъđ

r

a

er

р**-**

9

d :s i

сe

5

ons

<u>n</u>-

*x* -

nd

3

-

٦

:n

0

÷

al

se

iter

Shot	Total Yield	Shot Site	Area*	Fissio	n Yield		Fallout	
	Mt		mi <sup>2</sup>	Mt	met	mc‡	pct‡	pct§
Tewa	_5.0	Reef	43,500	£		6,458	24	28
Navajo	and and	Water	10,490	<u>i</u>	Ì	970	36, 58	50
Zuni	3.5	Land	13,400		S	1,540	46	48
Cherokee		Air	None	3	2	None		—
Flathead		Water	11,000	<u> JC</u>	<u>_</u>	275	15	29

\* Area out to 0.1 mr/hr at H + 24 hours and 3 feet above surface.

- \* Based on material located within the surveyed area, Tables 3.3 through 3.6.

§ Based on extrapolated values, Figures 4.1 and 4.2.

**f** Flathead survey limited by aircraft contamination. Results based on estimated position of boundary.

of surface displacement is clearly visible, the enclosed area is approximately the same each day within the limits of measurement error.

The indications are that the survey results, properly related to mixing in the ocean volume, may be used for estimates of fallout density. The oceanographic surveys of Project 2.62 (SIO) provide more detailed study of the mixing function.

4.3.2 Estimates of Total Fallout. The fallout distribution from the aerial-survey estimates are plotted in Figures 4.1 and 4.2. The percentage of the total fission yield is displayed against the particular boundary isodose contour. These curves can then be extrapolated to the zero mr gamma contour and the estimate made of the total amount of fallout in the local area. The conclusions must be applied judiciously, because the estimates are not between measured values, but an extrapolation beyond the survey area.

The estimates are summarized in Table 4.1. The megacurie summaries represent the material within the EOB of the surveys, and the percentage fallout is based on the percentage of the total yield found within the surveyed area and on the values extrapolated in Figures 4.1 and 4.2. Natural radiation background and the residual background from previous shots vary from place to place. Because small fluctuation in the radiation detector readings are an indication of the boundary of the fallout, variations in background will affect the outer boundary estimates (Section 1.3.4). While this does not vary the position of the isodose lines, it does affect the position of the EOB and the estimates contained in the fallout summations. **DOE ARCHIV** 

Of the isotopes produced by neutron activation, two are primarily important in contributing to the gamma activity: Np<sup>239</sup> and Na<sup>21</sup>. The Np<sup>239</sup> contribution to aerial-survey measurements is small, because of the low energy of its gamma photon (Section 1.3.3).

The Na<sup>24</sup> emits high-energy gamma photons and can increase the gamma dose rate measured by aerial survey appreciably in the period from 5 to 100 hours (Section 1.3.3). Measurable





## Chapter 5 CONCLUSIONS and RECOMMENDATIONS

#### 5.1 CONCLUSIONS

The gamma radiation field over fallout-contaminated ocean was successfully surveyed by aerial detectors after Shots Zuni, Navajo, and Tewa. No fallout was found in the sea following Shots Cherokee and Mohawk.

Contamination on the aircraft determined the minimum detectable dose rate over the sea. Airborne radioactive material was encountered by the survey aircraft on D+1 day after Shot Flathead. These isodose plots therefore were limited to the relatively hot close-in fallout area.

5.1.1 Altitude Absorption. The field measurements of gamma dose rate at various altitudes over contaminated land and water areas agree with the relationships developed by theoretical calculations.

A 500-kev average gamma-emission energy was assumed, and this is substantiated by the ratio of readings of an energy-dependent detector compared to the readings of an energy-independent detector.

5.1.2 Fallout Distribution. A land-equivalent isodose plot may be inferred from the surveys over the sea. For example, a fallout density of 0.36 megacurie/naut mi<sup>2</sup>, on a land surface, will result in 1 r/hr at 3 feet from the surface. The same fallout density in the sea, after mixing, will result in 0.88 mr/hr at 3 feet from the surface (Section 1.3.4). However, the location of the isodose contours must be corrected to the location of the ocean surface at the time of fallout. The repeat surveys on subsequent days after the shot indicate the distortion of the contours, and the direction and magnitude of the ocean currents at the surface. The 0.1 r/hr gamma dose rate at Parry Island 24 hours after Shot Tewa agreed with its location between the 0.025 and 0.25 r/hr land-equivalent isodose contours determined from the aerial survey over the sea.

The land-equivalent conversion is based on uniform mixing of the fallout in the sea to a depth of 60 meters. Samples of sea water from various depths provided the data on which this estimate was based. While only a few stations could be sampled, the reproducibility of the areas enclosed by the isodose contours from aerial surveys on succeeding days indicate that the mixing becomes stabilized for a reasonable number of days after a shot.

5.1.3 Material-Balance Estimates. The conversion from fission-product contamination density to gamma dose rate could not be conclusively validated from the data available. However, estimates were made based on the calculated factors. The measurements show no detectable fallout from the air burst, Shot Cherokee.

The two water-surface shots, Flathead and Navajo, deposited percent, respectively, of their fission-product yield as fallout in the local area

Shot Zuni was fired on a land site, and its fallout accounted for second of its fissionproduct yield. It is possible that the soil picked up in the fireball provides relatively heavy particles which, on condensation, fall to the surface faster than the products resulting from a water shot.

The fallout from Shot Tewa, fired on a reef site, was approximately 30 percent of the total yield.

**DOE** ARCHIVES

56

SECRET

#### 5.2 RECOMMENDATIONS

Operationally,  $\_$ -day aerial surveys provide little information because of the necessity of avoiding active fallout. Even light contamination on an aircraft hinders surveys on later days when the intensity from the sea is reduced by radioactive decay. Unless the aircraft can be decontaminated, aerial surveys should not be made on D-day.

With regard to instrumentation, a linear-scale radiation detector would provide more accurate and more readable recordings over water, where most of the gamma dose rates are slightly above the natural background of the sea and the aircraft. The logarithmic scale is essential for surveys over land, where a wide range of intensities must be measured.

61

**DOE ARCHIVES** 

# Appendix A DERIVATION of ALTITUDE ABSORPTION of GAMMA RADIATION

Keran O'Brien, Radiation Branch, Health and Safety Laboratory

The equation giving the dose rate above a hole in an infinite half-space that subtends an angle  $\theta^0$ , when the half-space is uniformly contaminated with a gamma emitter, is described in Reference 10 and is:

$$\mathbf{I}_{\nu} = \frac{\mathbf{E}}{2\sigma \mathbf{Y}} \Lambda(\mathbf{h}, \theta^{0})$$
 (A.1)

Where: E is the gamma energy emitted per cubic centimeter by the contaminant

 $\sigma$  is the density of the absorbing medium

h is the height of the detector, in meters, and

$$Y = \frac{\mu_1}{\mu_e}$$
, the ratio of the total attenuation co-

efficient to the energy absorption coefficient of the medium, corresponding to the source energy

For  $\Lambda$ :

$$\Lambda(\mathbf{h}, \theta^{\mathbf{0}}) = \frac{1}{u} \{ \mathrm{tu} \mathrm{E}\,\mathrm{i} \,(-\mathrm{tu}) + \mathrm{e}^{-\mathrm{tu}} \mathrm{B}(\mathrm{tu}) \}$$
(A.2)

 $t = \mu_t h$ ,  $u = \sec \theta^0$ , and B(tu) is a polynomial

The dose rate above a plane, similarly contaminated, can be obtained by the partial derivative of Equation A.1 to obtain an infinitesimal thickness of slab:

$$\frac{\partial I_{\nu}}{\partial h} dh = I_{p}$$
 (A.3)

This is:

$$I_{\mathbf{p}} = \frac{E}{2\sigma Y} \mu_{t} dh M(tu)$$
 (A.4)

with M(tu) =  $-E_i(-tu) + e^{-tu}[B(tu) - B'(tu) - 1]$  (A.5)

Where: 
$$B^{\dagger} = \frac{dB}{d(tu)}$$

The clearing on the surface also subtends on angle  $\theta$ .

For the case of radiation from water or land contaminated with fission products, seen by an aircraftmounted detector, a finite diameter of contamination on the surface is described by a half-angle sensitivity,  $\theta$ .

CASE I. Water contamination from Equation A. l.

$$\mathbf{L}(\mathbf{h}, \theta) = \Lambda(\mathbf{h}, \theta^{0}) - \Lambda(\mathbf{h}, \theta)$$
 (A.6)

and

$$\frac{E}{2\sigma Y} = \frac{E_0 j}{2\sigma Y}$$

where j is the disintegration per second per cubic centimeter and  $E_0$  is the average source energy.

$$I_{\nu} = \frac{E_0 j}{2\sigma Y} L(h, \theta)$$
 (A.8)

The constants may be converted to appropriate units to relate contamination density to gamma dose rate by:

$$K = \frac{cq\mu_{e} (3,600)}{W\mu_{t}} E_{0}$$
 (A.9)

Where: 
$$c = 3.7 \times 10^{10} \text{ (photons/sec)/m}^3$$
  
 $q = 4.8 \times 10^{-10} \text{esu}$   
 $\mu_e = 3.54 \times 10^{-5} \text{ cm}^{-1} \text{ (for water)}$   
 $W = 3.25 \times 10^{-5} \text{ Mev} (32.5 \text{ ev})$   
. 3,600 sec/hr  
 $10^6 \text{ cm}^3/\text{m}^3$ , and  
E<sub>0</sub> is assumed to be 0.5 Mev

Then:

$$I_{\nu} = \frac{0.3549}{2} C_{\nu} L(h, \theta^{0}) R/hr \qquad (A.10)$$

where  $C_{\mu}$  = curies per cubic meter.

$$J(h, \theta) = M(h, \theta^{0}) - M(h, \theta) \qquad (A.11)$$

and

$$\frac{\mu_{\rm t} E \, dh}{2\sigma Y} = \frac{\mu_{\rm e} E_0 K}{2\sigma} \tag{A.12}$$

where k represents disintegrations per second per square centimeter.

This reduces Equation A.4 to:

$$I_{p} = \frac{\mu_{e} E_{0} k}{2\sigma} J(h, \theta^{0}) \qquad (A.13)$$

With the constants converted to appropriate units as in Case I, and  $10^4\ {\rm cm}^2/{\rm m}^2.$ 

$$K = \frac{cq\mu_e(3,600)k}{W} E_0 \qquad DOE \text{ ARCHIVES}$$
(A.14)

$$I_p = 3.4427 C_p J(h, \theta^0) R/hr$$
 (A.15)

(A.7) where  $C_p$  = curies per square meter.



## Appendix B DETAILS of MAJOR INSTRUMENTS

#### B.1 AERIAL RADIATION DETECTOR, HASL TH-10-B output of the telemeter is a 1,000-cps tone, gated on and

The Top Hat aerial radiation detector is a scintillation detector utilizing plastic phosphors. The phosphors are coupled to photomultiplier tubes, and the integrated current output is amplified by a dc amplifier. The amplifier has a logarithmic response and covers a 4-decade range of radiation intensity. By switching between two photomultipliers which have different-size phosphors, two ranges of 4-decades each are achieved: Range A, 0.01 to 100 mr/hr, and Range B, 10 mr/hr to 100 r/hr.

The A phosphor is 3 inches in diameter and 3 inches high, and the B phosphor is  $1^{1}/_{8}$  inches in diameter and  $3_{8}$  inch high. The output of each range varies from 0 to 1 ma and drives a strip-chart recorder, Esterline Angus Co., AW. The radiation calibration of a typical unit is shown in Figure B.1. Both phosphors are collimated by an annular lead shield, which was added to reduce the effect of aircraft contamination.

For a more detailed description of the instrument, see Reference 11.

#### **B.2 ALTITUDE COMPENSATOR**

The surface radiation reading,  $R_3$  is related to the aircraft reading,  $R_{a/c}$ , by a constant,  $f_a$ , which depends on the height above the surface. Thus,  $R_3 = R_{a/c} \times f_a$ . However, the circuit current is related to the logarithm of  $R_{a/c}$ , and the altitude, h, is proportional to the logarithm of  $f_a$ . The indicated multiplication can be performed by the addition of the logarithms:

 $R_3 = I_a/c + kh$  (200 < h < 1,000)

### Where: I is a current measured in milliamperes k is a circuit constant

The altitude-compension circuit electrically adds an altitude signal, derived from the aircraft radio altimeter, APN-1, to the output of the detector circuit. The aircraft radiation reading is continuously modified for changes in flight altitude, and the surface readings remain proportional to the gamma intensity at 3 feet above the surface.

#### B.3 TELEMETER, HASL TT-3-X

The telemeter is connected in series with the stripchart recorder and converts its drive current, 0 to 1 ma direct current, to an alternating-current wave form suitable for transmission through audio circuits. The

output of the telemeter is a 1,000-cps tone, gated on and off within a 1-second cycle. The ratio of on to off time within the 1-second time interval is proportional to the input de signal. These bursts of 1,000 cps may be coupled directly into the microphone input of a radio transmitter or stored on an audio tape recorder.

A high-fidelity transmitter, U.S. Navy ART-13, was used in the P2V-5 aircraft. It has an output power rating of 100 watts. Continuous operation is not possible because of heat dissipation limitations. Also, the transmitted signal blocks the receivers in the aircraft. Therefore, the telemeter output, the gated 1,000-cps tone, is recorded on a tape recorder running at  $3\frac{3}{4}$ -in/ sec. The tape is then manually shifted to a playback recorder, which runs at 30-in/sec. The recording reel, containing up to 30 minutes of data, is played back through the radio transmitter in less than 4 minutes.

An electronically regulated power supply, HASL TB-6-A, supplies all the voltages to the telemeter and the detector control assembly. The regulators compensate for the varying 28-volt input power from the aircraft generators.

The telemeter central station is connected to the earphone output jack of a receiver, which is tuned to the transmitter frequency. The input to the central station has a noise filter, designed to reject 54 decibels of radio noise above the signal level. This is followed by a conventional ratemeter which converts the bursts of 1,000-cps tone to a deflection of the pen on a strip-chart recorder.

#### B.4 AUTOMATIC GAMMA MONITOR, HASL TN-4-C

The automatic gamma monitor is based on a detector similar to the Top Hat aerial radiation detector. A plastic phosphor is optically coupled to a photomultiplier, whose output is converted in a dc amplifier to a logarithmic response. The unit reproduces a radiation range from 1 mr/hr to 10 r/hr on a single scale. The output is continuously recorded on an Esterline Angus strip-chart recorder. The monitor operates on 115-volt, 60-cps current and is completely scaled in an immersionproof case.

#### **B.5 SCINTAMETER SURVEY METERS**

### **DOE** ARCHIVES

The scintameters are portable survey meters that are powered by dry batteries and are completely self-contained.





The TH-7-A uses the same phosphor and circuit as the Top Hat radiatio tector meter and has a nearly air-equivalent energy response. The unit has a logarithmic scale, calibrated from 1 mr/hr to 10 r/hr.

The standard high-sensitivity scintameter, TH-3-B uses a sodium iodide detector that has an energydependent dose-rate response (Figure B.2). It has a logarithmic scale, calibrated from 0.01 to 100 mr/hr.

#### B.6 GAMMA SPECTROMETER, HASL TM-10-A

The gamma spectrometer is a single-channel, automatic-sweep pulse-height analyzer. Its detector is a crystal of sectium iodide, thallium iodide activated, 4 inches in \_\_\_\_\_neter and 4 inches high. The circuits are designed to handle high pulse rates, and the ratemeter section is calibrated in seven ranges from 100 to 100,000 counts/sec. The base line may be selected as 3, 1.5, or 0.75 Mev full scale and swept automatically from 1 minute to 4 hours for the full-energy scan. Data is displayed on a Mosely Autograf 2, X-Y recorder.

The unit operates on 115-volt, 60-cps current. For helicopter use, external inverters must be supplied to invert the 28-volt current of the aircraft.

### **DOE** ARCHIVES

65



NEW CONTRACTOR CONDENSITY AND INCOME

# Appendix C ALTITUDE ABSORPTION MEASUREMENTS DURING PREVIOUS OPERATIONS

Aerial dose-rate measurements above contaminated areas have been abstracted from records of previous weapon tests. These data include surveys over land contaminated with old and with fresh fission products, and surveys over water containing fresh fission products.

Table C.1 contains data collected over land contaminated with old fission products, at the Nevada Test Site, between operations and prior to Operation Castle. curve, except the Plumbbob gamma dose rates that have been related to the surface measurement. Figures C.1 and C.2 are altitude plots for land and water, respectively. The agreement with the calculated attenuation curve is within the limits of error imposed by altitude measurement and instrument calibration. A single surface reading, i.e., 3-foot dose rate over land, usually deviates markedly from the value predicted from the readings at higher altitudes. This is a

## TABLE C.1 ALTITUDE ABSORPTION MEASUREMENTS OVER LAND, OLD FISSION PRODUCTS

Altituda		Absorption	of Radia	tion	
Annuae	1*	2	†	3‡	
ft	pct	mr/hr	pct	mr/hr	pct
3	100	4.3	57,128	4.3	50
50				2.0	40
100		_	_	1.8	36
200	25	0.79	22	1.0	22
400	_	0.56	13.5	0.75	15.5
500	10	0.40	11	0.38	8.2
800		0.11	4		

\* NTS, 1951, old shot site, scintilog TH-2, normalized from a series of ground and aircraft readings.

† Janet Island, Eniwetok Atoll, prior to Operation Castle, scintameter TH-3, P2V aircraft.

**‡** Janet Island, Eniwetok Atoll, prior to Operation Castle, scintameter TH-3, helicopter.

### DOE ARCHIVES

During Operations Teapot and Plumbbob, careful measurements were made 3 feet from the surface, in conjunction with simultaneous aerial measurements. Data abstracted from these surveys (Reference 12) are included in Table C.2.

Fresh fission products in water volume were examined during Operation Wigwam (Reference 4), and the altitude absorption measurements are contained in Table C.3.

All data have been normalized to the theoretical

function of the nonhomogeneous contamination on the small areas viewed close to the surface and the unevenness of the surface. The NTS (Table C.1, No. 1) and Plumbbob (Table C.2, Nos. 2 and 3) data are based on careful surface measurements, made by survey over an extended area and averaged; and the 3-foot value agrees with the predicted values. Measurements over water are difficult to obtain, because a ship will distort the radiation field. Data below 50 feet from sec surface are not available.

A 14144		A	bsorption c	of Radiatio	n	
Annuae	1	*	2	t	31	
ft	mr/hr	pct	mr/hr	pct	mr/hr	pet
3	10	705	250	100	100	100
50	6.3	49		—		
100	4.8	34		—		·
150	4.3	30				<u> </u>
200	3.3	23				<u> </u>
250	2.75	19				
300	2.35	17	31.7	12.7	15.9	16
350	1.85	13				
400	1.7	12		_		_
450	1.52	11	_			
500	1.7	12	21	8.4	8.6	8.6
550	1.3	9.2				
600	1.0	6.2		—		
700			13	5.2	4.8	4.8
800	0.76	5.7	_			—
900			6.9	2.8	2.7	2.7

# TABLE C.2ALTITUDE ABSORPTION MEASUREMENTS OVER LAND,<br/>FRESH FISSION PRODUCTS

\* Operation Teapot, 1955, NTS, Shot Turk.

† Operation Plumbbob, 1957, NTS.

**‡** Operation Plumbbob, 1957, NTS.

.

\$ 10 mr/hr, based on single surface reading at 3 feet.

Altitude	A	bsorption	of Radiation	
Annue	1*		2†	
ft	mr/hr	pct	mr/hr	pct
50	83	83		
100	72	72		
200	60	60	17	52
300	40	40	—	
400	35	35	15	32
600	20	20	10	18
800	10	10	6.1	10
1,000	5	5		

# TABLE C.3ALTITUDE ABSORPTION MEASUREMENTSOVER WATER, FRESH FISSION PRODUCTS

**DOE** ARCHIVES

\* Operation Wigwam, 1955, scintameter TH-3, helicopter.

† Operation Wigwam, 1955, Top Hat detector TH-10-A,

AD-5N aircraft.







# Appendix D ANALYTICAL DATA from SAMPLES of SEAWATER

Duplicate samples of sea water were furnished by the NRDL and the SIO. At the HASL, each sample was filtered and the remainder evaporated. The beta activities the general magnitude of this assumption is correct. for both particulate and salt fractions were determined by counting. These data were corrected for radioactive decay on the basis of the decay curves in Reference 7.

### **D.1 SURFACE SAMPLES**

The beta analysis, corrected to H+24 hours, is summarized in Tables D.1, D.2, D.3, and D.4, for Shots Zuni, Flathead, Navajo, and Tewa. The sampling locations were plotted on the aerial-survey isodose charts and the gamma intensity at each station was estimated by extrapolation between the isodose contours. Because Activities below 10 dis/min are not particularly valid, the gamma dose-rate values are estimated, further extrapolation may contain errors. The time of gamma survey and the time of sampling do not necessarily coincide, so the interviewing horizontal translation of the water mass can introduce displacement errors.

The surface activity, as beta disintegration per minute per liter, has been plotted against estimated gamma dose rate in Figure D.1. With the large variation of the observed data, it is not possible to confirm the calculated value of  $4.43 \times 10^{6}$  (dis/min)/liter for 1 mr/hr gamma at 3 feet. However, the results do indicate that

#### D.2 DEPTH SAMPLES

Particulate salt separation and beta analysis were performed on a group of depth samples supplied by Project 2.62 (SIO). The count-time corrections for radioactive decay were made to the mean of the counting period for all samples within a group. The data from Shots Flathead and Navajo are summarized in Table D.5, and from Shot Tewa in Table D.6.

These values are plotted in Figures D.2 and D.3. because they correspond to counting rates below the statistically reliable level. The surface activity for samples from Shots Flathead and Tewa are based on the average of several identical samples. The surface activity for Station N-17, after Shot Navajo, is based on a single sample and may not represent the actual surface conditions. A mixing depth of 60 meters is indicated by this data (Figure 3.26).

### DOE ARCHIVES

TABLE D.1 ANALYSIS OF SEA WATER SAMPLES, SHOT ZUNI

.

No. of Street, or other

Sector Sector

تركيني بتشقيه

للغالي فأكديا هماه

غملانى كيديجيني كتبير فزياريه

うちち アー・ファン・アー・アンションション ないない たいちょう たいちょう たいちょう ちょうしょう ちょうしょう ちょうしん ひょうしん ひょうしん

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		St	ation		ď	articula	ite		Salt		Total	Intensity	Chart
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		Latitude	Longitude	Lime	103	Time	106	10 <sup>3</sup>	Tlme	10 <sup>6</sup>	106		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	}			(die	s/min)/liter	hr	(dis/min)/liter at 24 hrs	(dls/min)/liter	۲	(dis/min)/liter at 24 hrs	(dis/min)/liter at 24 hrs	mr∕hr at 24 hrв	day
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-25	165-26	5/28-2200	20	161	0.19	264	272	3.96	4.15	1.0	1+Q
2065       165-16       5/38-1405       1       101       ND*       00       45       1.75       ND*       0.5         12-10       165-17       5/29-0100       27       117       300       2.47       1.28       0.05         11-00       165-12       5/29-0100       27       1.03       0.05		12-22	165-27	5/28-2300	46	162	0.43	604	272	9.06	9.49	1.0	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-06.5	165-39	5/28-1430	1	161	0.01	•UN				0.5	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					+QN			*UN					
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-19	165-17	5/29-0100	69	456	1.75	137	308	2.47	4.22	1.5	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		13-00	165-12	5/29-0800	57	163	0.54	36	274	0.54	1.08	0.05	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		13 - 00	165-12	5/29-1430	49	162	0.46	*CIN				0.05	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-04	165-12.5	5/29-1900	2	161	0.02	9	308	0.11	0.13	0.05	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		13-04.7	165-12.5	5/29-2345	31	163	0.29	4	308	0.07	0.36	0.05	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		11-27	165-08.2	5/28-1300	0.7	209	0.01	*QN				0.025	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		11-45.1	165-08.2	5/28-1650	5	210	0.05	6	309	0.16	0.21	0.2	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-10	165-27.8	5/28-1950	43	210	0.43	52	309	0.94	1.37	1.0	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-13.8	165-53	5/29-0015	5	210	0.05	133	309	2.39	2.44	0.12	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-46.1	166-01.3	5/29-1310	41	210	0.41	8	309	0.14	0.55	0.12	
<b>Z</b> 11-50 165-04 5/28-1720 39 234 0.41 72 310 1.30 1.71 1.5 13-06 165 045 5/30-1100 2 161 0.02 2 309 0.07 0.11 0.08 0.08 13-06 165 045 5/30-0725 6 210 0.02 0.03 0.07 0.01 0.00 0.08 13-37 163-40 2 5/30-0725 6 210 0.02 15 15 13-46 164-33 5/30-1430 15 235 15 165 0.19 3.0 0.07 0.01 0.008 0.08 13-47 163-47 5/30-1430 15 235 15 165 0.19 3.0 0.07 0.01 0.008 15 13-47 163-47 5/30-1430 15 235 15 165 0.19 3.0 0.07 0.01 0.008 15 13-47 163-47 5/30-1430 15 235 15 165 0.19 3.0 0.07 0.03 0.15 15 13-48 164-56 5/31-1000 1.9 200 0.01 ND* 309 0.07 0.28 0.15 D+3 13-115 164-56 5/31-1000 1.9 200 0.01 ND* 100 0.01 0.05 11-10.03 13-115 164-56 5/31-1000 1.9 200 0.01 ND* 100 0.01 0.05 11-10.03 13-115 164-56 5/31-1010 5.3 211 0.02 3.9 309 0.07 0.03 0.15 0.15 12-33 13-115 164-56 5/31-1010 5.3 211 0.02 3.9 309 0.07 0.03 0.15 0.15 12-33 13-115 164-56 5/31-1010 5.3 211 0.02 3.9 309 0.07 0.03 0.15 0.15 12-33 13-115 164-56 5/31-1010 5.3 211 0.02 3.14 3.78 0.31 0.03 0.01 0.15 12-33 12-33 165-93 5/11-1010 13 211 0.02 24 3.09 0.03 0.01 0.01 0.15 12-33 15 2.12 0.04 3.0 23 0.05 0.01 0.01 0.15 12-33 165-93 5/11-1010 13 211 0.01 23 11 0.02 24 3.07 0.05 0.01 0.01 0.15 12-33 165-93 5/11-1010 13 211 0.01 2 21 0.01 0.01 0.03 0.02 0.01 0.01 0.01 0.01 0.01 0.01 0.01		11-40.3	165-35.2	5/28-1250	0.06	220	0.001	1.3	3.39	0.03	0.03	0.5	
13-06       15-045       5/30-1100       2       161       0.02       2       309       0.04       0.06       0.08       0.04         13-06.4       155-02       5/30-1140       2       161       0.02       3       309       0.07       0.01       0.08       0.04         13-37       153-102       5/30-1735       6       115       0.07       0.01       0.08       0.07       0.01       0.08         13-47       153-47       5/30-1300       15       235       15       381       0.11       0.08       0.07       0.01       0.08       0.09         13-47       153-47       5/30-1300       15       235       15       381       0.07       0.11       0.08       0.09       0.07       0.01       0.08       0.09       0.09       0.09       0.07       0.08       0.09 <td>N</td> <td>11-59</td> <td>165 - 04</td> <td>5/28-1720</td> <td>39</td> <td>234</td> <td>0.41</td> <td>72</td> <td>310</td> <td>1.30</td> <td>1.71</td> <td>1.5</td> <td>-</td>	N	11-59	165 - 04	5/28-1720	39	234	0.41	72	310	1.30	1.71	1.5	-
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-06	165-04.5	5/30-1100	2	161	0.02	2	309	0.04	0.06	0.08	D + 2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-06.4	165-02	5/30-1450	2	161	0.02	e	309	0.05	0.07	0.08	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-08.5	164 - 59	5/30-2200	4	165	0.04	4	309	0.07	0.11	0.08	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		13-37	163-40.2	5/30-0725	6	210		+QN				Low	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		13-46	164-33	5/30 - 1430	15	235		15	381			Low	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-47	163-47	5/30-1900	*UN			*UN				Low	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		13-09	164-58.5	5/31-0200	21.5	165	0.19	3.8	309	0.07	0.26	0.15	D+3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-11.5	164-55	5/31-0815	3.1	165	0.03	*UN				0.15	
13-12.5       164-56       5/31-1415       1.3       200       0.01       ND*         13-13       164-52       5/31-1415       1.3       209       0.04       4.8       309       0.31       0.13       0.15         12-52.7       165-45.2       5/31-100       5.3       210       0.05       14       378       0.31       0.36       0.13       0.15         12-37.8       165-49.5       5/31-0100       5.3       211       0.20       24       309       0.43       0.63       0.25         12-333       165-90.4       5/31-0100       24       211       0.20       24       309       0.43       0.63       0.75         12-333       165-90.4       5/31-1100       13       211       0.13       211       0.13       212       0.61       130       0.64       3       0.65       3.77       0.64       3       3.72       0.25       0.75		13-11.5	164-55	5/31 - 1000	1.9	200	0.02	3.9	309	0.07	0.09	0.15	
13-13 $164-52$ $5/31-1830$ $4.1$ 209 $0.04$ $4.8$ 309 $0.09$ $0.13$ $0.15$ $12-52.7$ $165-45.2$ $5/31-0100$ $5.3$ $210$ $0.05$ $14$ $378$ $0.36$ $0.63$ $0.25$ $12-37.8$ $165-49.5$ $5/31-0610$ $5.3$ $210$ $0.20$ $24$ $309$ $0.43$ $0.63$ $0.25$ $12-33.8$ $165-94.5$ $5/31-0610$ $2.4$ $309$ $0.43$ $0.63$ $0.75$ $0.75$ $12-33.8$ $165-94.5$ $5/31-0810$ $24$ $211$ $0.23$ $0.12$ $0.63$ $0.75$ $0.75$ $0.75$ $0.75$ $12-33.8$ $165-94.5$ $5/31-1106$ $13$ $211$ $0.13$ $21$ $0.13$ $21$ $0.64$ $0.75$ $0.75$ $0.75$ $0.75$ $0.75$ $0.76$ $0.75$ $0.76$ $0.76$ $0.76$ $0.76$ $0.76$ $0.76$ $0.76$ $0.75$ $0.76$ $0.76$ $0.76$ $0.76$ $0.76$ $0.76$ $0.76$		13-12.5	164-56	5/31-1415	1.3	200	0.01	*QN				0.15	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		13-13	164-52	5/31-1930	4.1	209	0.04	4.8	309	0.03	0.13	0.15	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-52.7	165 - 45.2	5/31-0100	5.3	210	0.05	14	378	0.31	0.36	0.50	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-37.8	165 - 49.5	5/31 - 0300	20	211	0.20	24	309	0.43	0.63	0.25	
12-33       15-93       15       375 $0.27$ $0.64$ 3         12-33       164-40       5/31-1110       13       21 $0.13$ 21 $0.13$ $0.66$ $3.72$ $0.64$ $3$ 12-20       164-40       5/31-1110       13       21 $0.13$ 21 $0.13$ $0.66$ $0.66$ $0.66$ $0.66$ $0.66$ $0.66$ $0.66$ $0.79$ $0.66$ $0.66$ $0.30$ $0.12-10.3$ 164-50.8       5/31-1435 $4.1$ $2.12$ $0.04$ $2.55$ $374$ $4$ $0.10$ $0.30$ $0.12-10.3$ 164-50.8       5/31-1435 $4.1$ $2.12$ $0.04$ $2.55$ $374$ $4$ $0.10$ $0.30$ $0.12-39.7$ $165-57$ $6/1-0015$ $17.8$ $2.35$ $0.18$ $1.29$ $3.12$ $0.26$ $0.10$ $0.25$ $0.15$ $165-57$ $6/1-0130$ $11.5$ $2.35$ $0.12$ $3.0$ $3.12$ $0.26$ $0.25$ $0.15$ $0.12$ $0.12$ $0.12$ $0.12$		12-43.9	165-30.2	5/31-0610	24	211	0.25	6	309	0.20	0.45	0.75	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		12-33	165-09.4	5/31-0830	36	211	0.39	15	375	0.27	0.64	9	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		12-33	164-40	5/31 - 1110	13	211	0.13	21	310	0.46	0.59	0.6	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1	J 2-20	164 - 59.3	5/31-1320	60	212	0.61	130	374	2.86	3.47	4	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\mathcal{L}^{\prime}$	712-10.3	164-50.8	5/31-1435	4.1	212	0.04	2.5	379	0.06	0.10	0.30	
V12-44     165-59     6/1-0015     17.8     235     0.18     29     382     0.64     0.82     0.25       V12-33     165-57     6/1-0130     11.5     235     0.12     30     382     0.66     0.78     0.2       V12-33     165-57     6/1-0130     11.5     235     0.12     30     382     0.66     0.78     0.2	ل ب	12-39.7	163-38	5/31 - 2045	1.8	210	0.02	+CIN				0.15	
Y12-33 165-57 6/1-0130 11.5 235 0.12 30 382 0.66 0.78 0.2 Alt	2	12-44	165-59	6/1 - 0015	17.8	235	0.18	29	382	0.64	0.82	0.25	
ĠHVE	<i>6</i> 1,59	<b>1</b> 2-33	165-57	6/1-01:30	11.5	235	0.12	30	382	0.66	0.78	0.2	
HVE	LA 문	بنع											
VE	11	111											
	¥ Ľ												

70

TABLE D.2 ANALYSIS OF SEA WATER SAMPLES, SHOT FLATHEAD

	<u> </u>				_	·····	Beta				Gam	mə
	50	tion		P	articula	ite		Salt		Total	Intensity	Char
Number	Latitude	Longitude	11me -	103	Time	106	101	Time	106	106		-
			(d	is/min)liter	hr	(dis/min)/liter	(dis/min)/liter	hr	(dis/min)/liter	(dis 'n.in) liter	mr hr	day
						at 24 hrs			at 24 hrs	at 24 hrs	at 24 hrs	
<b>F</b> -1	11-30	165-11.3	6/12-2400	9.7	369	0.20	21.7	370	0.46	0.51	0.03	D + 1
F-2	12-10	165-31.3	6/13-1200	14.8	185	0.15	7.8	190	0.08	0.19	0.04	1
F-2				6.4	185	0.07	13.3	190	0.13			
F-2				21.6	185	0.19	11	188	0.11			
F-2				4.7	185	0.05	7.8	188	0.08			
F-3	12-10.2	165-31	6/13-2300	148	185	1.50	55	187	0.56	0.32	0.04	
F-3				9	185	0.09	23	188	0.23			
F-3				8.1	185	0.08	18	188	0.18			
M-1	11-30.5	164-53.8	6/12-1730	ND*							0.15	
M-2	12-30	165-14.2	6/13-1220	ND *							0.07	
M-3	12-44	165-31.2	6/13-1700	ND*							0.05	ļ
S-1	11-36	165-11	6/12-2310	9.9	368	0.21	11	368	0.23	0.43	0.15	
S-1				3.7	368	0.08	16	368	0.34			
S-2	11-52	165-23	6/13-0130	23.7	369	0.5	49	369	1.03	1.53	0.15	ł
S-3	11-52	165-19	6/13-1400	ND*							0.23	
S-4	11-51	165-20	6/13-1700	ND*							0.2	1
S-5	11-53	164-56	6/13-1930	ND*							0.05	
¥3-1	12-04	165-26	6/12-2015	22.5	91	0.12	132	91	0.69	0.81	0.22	
¥3-2	12-08	165-28	6/13-0115	25	93	0.14	222	93	1.24	1.38	0.18	[
¥4-2	12-45	166-01	6/13-0730	25	92	0.14	157	93	0.88	1.02	0.03	
¥4-3	12-41	166-05	6/13-0919	49	91	0.26	222	92	1.20	1.46	0.025	<b>†</b>

\* No data.

TABLE D.3 ANALYSIS OF SEA WATER SAMPLES, SHOT NAVAJO

	510	tion					Beta				Gam	ma
Number	Totiludo	Langitudo	Time	Pa	articul	ate		Salt		Total	Intensity	Churt
Number	Latitude	Longitude	Time -	10 <sup>3</sup>	Time	106	103	Time	105	106		
			(d	is/min}/liter	br	(dis/min//liter	(dis/min)/liter	hr	(dis/min)/liter	(dis/min)/liter	mr/hr	day
						at 24 hrs			at 24 hrs	at 24 hrs	at 24 hrs	
¥3-1	12-10	165-19	7/11-1615	218	82	1.03	1,125	82	5.29	6.32	0.125	D+1
¥3-2	11-59.5	165-15.5	7/11-2330	585	78	2.46	506	78	2.13	4.59	0.8	1
¥3-3	11-59.5	165-15.5	7/12-0005	498	79	2.14	383	79	1.65	3.79	0.8	i i
¥3-4	11-58	165-15	7/12-1421	506	83	2.43	383	83	1.84	4.27	0.8	i i
¥3-5	11-56	165-15.5	7/12-1750	487	80	2.19	298	80	1.34	3.53	0.8	
¥3-6	12-00	165-15	7/12-2150	328	81	1.51	259	81	1.19	2.70	0.8	ł
N-1	11-21.3	165-14	7/11-1341								Low	İ
N-2	11-34.5	165-09	7/11-1920								0.025	
N-3	11-47.2	165-07.3	7/11-2130	102	203	1.04	213	203	2.17	3.21	1.0	
N-4	11-57	165-17.5	7/12-0030								0.5	1
N-5	11-58.5	165-13	7/12-0315								0.3	1
N-6	11-58.3	165-12.3	7/12-0800								0.3	
N-7	11-59	165-08	7/12-1330	18.4	203	0.19	45.3	203	0.46	0.65	0.15	i
N-8	11-59.5	165-09	7/12-1700	-							0.15	1
M-1	11-38.5	164-53.4	7/11-2000	92	206	0.94	94	206	0.96	1.90	0.8	i
M-2	11-38	164-43.6	7/11-2130	77	206	0.79	123	206	1.25	2.04	0.6	
M-3	11-37.5	164-37.5	7/12-0018	105	206	1.07	81	206	0.33	1.90	0.8	
M-4	12-03	163-18.2	7/12-1830			1.07				1.00	0.01	
N-9	11-44.8	165+16.2	7/13-000							DOF	LARC	HJYF
N-10	11-50	165-14.4	7/13-0810								10	
N-11	11-46.5	165-14	7/13-1035	32	196	0.22	84	196	0.85	1 17	1.5	1
N-12	11-43.2	165+17.2	7/13-1330		100	V.02	ψ <b>η</b>	100	V-0 V	A-1 /	1.0	1
N-13	11-34.0	165-11	7/13-2110	46	204	0 47	80	204	0.92	1 20	1.0	
M-5	12-44 3	162-40	7/13-0100	10	204	0.11	30	204	0.52	1.35	0.20	1
M-6	12-77.0	164-41 4	7/13-0900								0.03	
	12-20.1	104-41.4	1,13-0900								0.1	1

71

÷

10 <sup>6</sup> 115/min)/liter (dis// at 24 hrs 2.4 1.65 3.57 6.45 1.09 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.57 0.99 0.99 0.99 0.99 0.99 0.99 0.99 0.99 0.99 0.10 0.	TIme hr (d hr (d 264 264 264 473 264 473 334 334 334 334 334 334 334 334 33	10 <sup>3</sup> (dis/min)/liter 160 110 238 42 43 42 43 42 42 43 52 52 52 52 52 157 157 157 157 157 157 157 157 157 157	1100 1100 1100 1100 1100 1100 1100 110	1 ( 1me, A 7 / 21-2 7 / 22-0 7 / 22-1 7 / 22-2 7 / 22-0 7 / 22-0 7 / 22-1 7 / 22-2 7 / 22-2 7 / 22-2	Longlude 11me, A 165-16 7/21-2 165-15 7/22-0 165-13.5 7/22-1 165-13.5 7/22-2 165-13.2 7/22-0 165-13.2 7/22-0 165-13.2 7/22-1 165-12 7/22-1 165-10.5 7/22-2 165-06.2 7/21-1 165-06.2 7/22-0 164-40.0 7/22-0
iis/min)/liter (dis// at 24 hrs 2.4 1.65 3.57 6.45 6.45 1.09 0.43 0.43 0.43 0.43 0.43 0.43 0.99 2.98 3.74 2.98 3.74 2.93 3.74 2.93 2.57 0.14 1.81 1.81 2.93 2.57 0.14	hr (d 264 264 264 264 264 473 264 334 334 334 334 334 334 334 334 334 3		(dis/min)/liter 160 110 238 42 42 42 42 157 157 157 157 157 157 153 153 123 95 123 123	(dis/min)/liter       7/21-2200     160       7/22-0215     110       7/22-1310     238       7/22-1310     238       7/22-1310     238       7/22-1310     238       7/22-1310     238       7/22-1310     247       7/22-0330     247       7/22-1245     197       7/22-1245     197       7/22-1245     137       7/22-1245     137       7/22-1245     137       7/22-1245     137       7/22-1245     137       7/22-1245     137       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123       7/22-1245     123	(dis/min)/liter       165-16     7/21-2200       165-15     7/22-0215       165-13.5     7/22-0215       165-13.5     7/22-1310       165-13.5     7/22-1310       165-13.5     7/22-0330       165-13.2     7/22-0330       165-13.2     7/22-0330       165-13.2     7/22-0330       165-13.2     7/22-0330       165-13.2     7/22-0330       165-13.2     7/22-0330       165-13.2     7/22-1245       165-12.5     177       165-12.5     173       165-12.5     173       165-10.5     7/22-1245       165-10.5     7/22-1245       165-10.5     7/22-1245       165-10.5     7/22-1245       165-10.5     7/22-1245       165-10.5     7/22-1245       165-10.5     7/22-0100       165-10.5     7/22-0205       165-00.5     173       165-00.5     7/22-0153       165-00.5     7/22-0153       165-00.5     7/22-01633       165-00.5     7/22-0153       165-00.5     123       165-00.5     135       165-00.5     135       165-00.5     135       164-00.0     7/22-0647
2.4 1.65 6.45 1.08 2.57 3.3.38 2.99 2.93 2.99 4.69 2.93 2.93 2.93 2.57 3.75 4.6 5.93 2.57 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4	264 264 233 233 247 233 244 233 244 233 244 254 254 254 254 254 254 254 254 254		160 110 238 430 42 47 52 157 157 157 157 155 155 98 98	7/21-2200 160 7/22-0215 110 7/22-1310 238 7/22-1845 430 7/22-0100 42 7/22-0330 247 7/22-0330 247 7/22-1245 157 177 7/22-1245 197 177 7/22-1245 123 95 154 173 7/22-255 95 173 7/22-255 95 154 135 154 135 152 151 0 2.8 152 2.8 172 151 0 2.8 152 2.8 153 151 0 2.8 154 151 151 151 151 151 151 151 151 151	165-16 $7/21-2200$ 160165-15 $7/22-0215$ 110165-13.5 $7/22-0215$ 110165-10.5 $7/22-1310$ 238165-10.5 $7/22-1845$ 430165-10.5 $7/22-0300$ 16165-13.2 $7/22-0330$ 247165-13.2 $7/22-0300$ 157165-13.2 $7/22-0900$ 157165-13.2 $7/22-0900$ 157165-10.5 $7/22-1245$ 197165-10.5 $7/22-1245$ 173165-10.5 $7/22-1245$ 135165-10.5 $7/22-0200$ 154165-06.2 $7/22-0015$ 98164-40.0 $7/22-0015$ 98164-07.2 $7/22-0047$ 123
1.65 3.57 6.45 7.08 1.08 3.3.99 9.99 2.93 1.84 1.81 2.93 1.84 2.93 1.84 2.93 2.93 2.93 2.93 2.93 2.93 2.93 2.57 2.93 2.57 5.66 5.66 5.67 5.67 5.67 5.67 5.67 5	2264 2264 2333 2332 2544 2564 2564 2564 264 264 264 264 264 264 264 264 264 2		110 238 430 42 42 54 52 52 157 177 177 173 173 173 173 173 173 95 98 98	7/22-0215 $7/22-1310$ $7/22-1345$ $7/22-1345$ $7/22-054$ $7/22-0330$ $16$ $7/22-0330$ $247$ $7/22-0900$ $157$ $7/22-1245$ $177$ $7/22-1245$ $177$ $7/22-2255$ $123$ $955$ $173$ $7/22-2255$ $1335$ $7/22-0015$ $98$ $7/22-0015$ $98$ $7/22-0015$ $98$ $7/22-0015$ $98$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
3.57 6.45 1.08 9.64 3.3.36 9.99 9.29 1.84 1.81 2.93 1.84 2.93 1.84 2.93 1.84 2.93 2.93 2.93 2.93 2.93 2.93 2.93 2.93	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		238 430 72 42 42 157 157 157 157 153 95 135 98 123	7/22-1310 $7/22-1845$ $7/22-1845$ $7/22-054$ $7/2$ $7/22-0300$ $16$ $1/7$ $7/22-0900$ $157$ $7/22-1245$ $177$ $7/22-1245$ $173$ $7/22-2255$ $173$ $177$ $7/22-2255$ $95$ $173$ $7/22-2255$ $95$ $173$ $7/22-2255$ $95$ $173$ $7/22-2255$ $95$ $173$ $7/22-2015$ $98$ $7/22-0015$ $98$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
6.45 1.08 0.99 2.398 2.999 2.51 2.93 2.55 2.93 2.55 2.55 2.55 2.55 2.55 2.55 2.55 2.5	264 264 456 456 3334 3334 3334 3334 3334 3334		430 72 42 16 52 177 177 177 177 177 177 177 177 177 17	7/22-1845 430 $7/22-2054 72$ $7/22-0100 42 16$ $7/22-0330 247$ $7/22-0900 157$ $7/22-1245 197$ $7/22-2255 123$ $7/22-2255 123$ $7/22-2255 123$ $177$ $7/22-2255 123$ $177$ $7/22-2255 123$ $177$ $7/22-2255 123$ $177$ $7/22-2255 123$ $177$ $7/22-1240 129$ $9$ $7/22-015 98$ $7/22-1510 2.8$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
1.08 1.09 4.69 2.99 2.324 2.93 1.81 2.93 1.81 2.93 1.81 2.93 1.81 2.93 2.57 3.14 2.93 1.81 2.93 1.81 2.93 1.81 2.93 1.81 2.93 1.81 2.93 2.93 2.93 2.93 2.93 2.93 2.93 2.94 2.63 2.94 2.63 2.94 2.64 2.64 2.64 2.64 2.64 2.64 2.64 2.6	264 456 456 334 334 334 334 334 334 334 334 234 264		72 42 54 54 55 157 157 157 157 157 157 157 123 98 98	7/22-2054 72 $7/22-0100 42$ $16$ $7/22-0330 247$ $52$ $7/22-0900 157$ $7/22-1245 197$ $7/22-1245 197$ $7/22-2255 123$ $95$ $173$ $7/22-2255 123$ $95$ $173$ $7/22-0015 98$ $7/22-0015 98$ $7/22-0151 2.8$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
1.09 6.43 3.36 9.99 3.29 2.93 1.81 2.93 2.93 2.93 2.93 2.93 2.93 2.93 2.93	456 473 334 334 3334 3334 3334 264 264 264		42 16 247 57 157 177 173 173 135 98 98 123	7/22-0100 42 16 16 16 16 7/22-0330 247 52 7/22-0900 157 7/22-1245 197 7/22-2255 123 95 173 7/22-2255 123 95 173 7/22-0015 9 8 7/22-0015 98 7/22-1510 2.8 100 2.8 100 100 100 100 100 100 100 100 100 10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
0.43 4.69 2.98 3.76 3.76 4.69 2.93 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1	473 334 3334 3334 3334 455 3334 465 264 46 264 46 264 264 264 264 264 264 2		16 247 52 177 177 173 173 173 123 98 98 123	16 7/22-0330 247 52 7/22-0900 157 7/22-1245 197 7/22-2255 123 95 173 173 177 177 177 173 173 173 173 173	16         165-13.2         7/22-0330         247           165-13.2         7/22-0900         157           165-13.2         7/22-1245         197           165-12         7/22-1245         197           165-10.5         7/22-1245         197           165-10.5         7/22-2255         123           165-10.5         7/22-2255         123           165-06.2         7/22-015         95           164-40.0         7/22-0015         98           164-07.2         7/22-0015         98
4.69 0.99 3.76 3.75 4.69 1.81 1.81 1.81 1.44 1.44 1.65 1.81 1.81 1.81 1.81 1.81 1.81 1.81 1.8	334 334 3334 3334 3334 3334 56 4 56 4 56		247 52 177 177 173 173 173 123 98 98 123	7/22-0330 247 52 7/22-0900 157 7/22-1245 197 7/22-1245 173 7/22-2255 123 95 173 7/22-2255 123 95 17/22-0015 98 7/22-0647 123 7/22-0647 123 7/22-1510 2.8	165-13.2     7/22-0330     247       165-13.2     7/22-0300     157       165-12     7/22-1245     197       165-12.5     7/22-1245     197       165-10.5     7/22-1245     123       165-10.5     7/22-2255     123       165-0.6.2     7/22-2255     123       165-06.2     7/22-02015     98       164-07.2     7/22-0015     98       164-07.2     7/22-0615     98
0.99 2.98 3.74 3.29 2.34 2.93 2.93 2.93 2.181 1.81 2.93 2.93 2.93 2.93 2.93 2.93 2.93 2.93	334 334 334 334 334 264 264 264 264 264 264 264 264 264 26		52 157 177 177 173 173 173 95 135 98 123	52 7/22-0900 157 7/22-1245 197 7/22-2255 123 95 154 135 154 135 154 135 17/22-0015 98 7/22-0647 123 7/22-1510 2.8	52       52         165-13.2       7/22-0900       157         177       177         165-12       7/22-1245       197         165-10.5       7/22-1255       123         165-10.5       7/22-2255       95         165-06.2       7/21-1930       9         165-06.2       7/22-0015       98         164-00.0       7/22-0647       123
2.98 3.36 3.74 2.34 2.93 2.93 2.93 2.93 2.93 2.93	3334 3334 3334 3334 3334 264 264 264 264 264 264 264 264 264 26		157 177 197 173 123 95 135 135 123	7/22-0900 157 7/22-1245 197 7/22-1245 197 7/22-2255 123 95 95 123 95 154 154 135 154 135 7/22-0015 98 7/22-0015 98 7/22-0015 98 7/22-1510 2.8	165-13.2     7/22-0900     157       165-12     7/22-1245     197       165-10.5     7/22-1255     123       165-10.5     7/22-2255     95       165-06.2     7/21-1930     9       165-06.2     7/21-1930     9       164-40.0     7/22-0015     98       164-07.2     7/22-0647     123
3.36 3.74 3.29 2.34 2.93 2.53 1.81 1.81 1.81 2.93 2.54 2.93 2.16 2.16 2.16 2.16 2.16 2.16 2.16 2.16	334 334 334 334 334 334 264 264		177 197 173 173 95 135 98 123	7/22-1245 197 7/22-2255 197 7/22-2255 123 95 154 135 7/21-1930 9 7/22-0015 98 7/22-1510 2.8	177           165-12         7/22-1245         197           165-10.5         7/22-2255         123           165-10.5         7/22-2255         95           165-06.2         7/21-1930         9           164-40.0         7/22-0015         98           164-07.2         7/22-0015         98
3.74 3.29 2.34 2.93 2.57 2.57 1.47 1.47	334 334 334 334 334 264		197 173 95 154 135 9 88 123	7/22-1245 197 7/22-2255 123 95 154 154 135 7/21-1930 9 7/22-0647 123 7/22-1510 2.8	165-12     7/22-1245     197       165-10.5     7/22-1245     123       165-10.5     7/22-2255     123       154     154       165-06.2     7/21-1930     9       164-40.0     7/22-0015     98       164-07.2     7/22-0647     123
3.29 2.34 2.93 2.57 1.47 1.47	334 334 334 334 334 264		173 123 95 154 135 98 123	173 7/22-2255 123 95 154 154 135 7/21-1930 9 7/22-0015 98 7/22-0647 123 7/22-1510 2.8	173 165-10.5 7/22-2255 123 95 154 154 165-06.2 7/21-1930 9 164-40.0 7/22-0015 98 164-07.2 7/22-0647 123
2.34 1.81 2.93 0.14 1.47 1.47	334 334 334 334 264 264		123 95 154 135 98 123	7/22-2255 123 95 154 154 135 7/21-1930 9 7/22-0015 98 7/22-0647 123 7/22-1510 2.8	165-10.5         7/22-2255         123           95         95           154         154           165-06.2         7/21-1930         9           164-40.0         7/22-0015         98           164-07.2         7/22-0647         123
1.81 2.93 2.57 0.14 1.47 1.85	334 334 334 264 264		95 154 135 98 123	95 154 135 7/21-1930 9 7/22-0015 98 7/22-1510 2.8	95 154 154 145-06.2 7/21-1930 9 164-40.0 7/22-0015 98 164-07.2 7/22-0647 123
2.93 2.57 0.14 1.47 1.85	334 334 264 264		154 135 9 123	154 135 7/21-1930 9 7/22-0015 98 7/22-0647 123 7/22-1510 2.8	154 135 165-06.2 7/21-1930 9 164-40.0 7/22-0015 98 164-07.2 7/22-0647 123
2.57 0.14 1.47 1.85	334 264 264		135 9 123	135 7/21-1930 9 7/22-0015 98 7/22-0647 123 7/22-1510 2.8	135 165-06.2 7/21-1930 9 164-40.0 7/22-0015 98 164-07.2 7/22-0647 123
0.14 1.47 1.85	264 264		9 98 123	7/21-1930 9 7/22-0015 98 7/22-0647 123 7/22-1510 2.8	165-06.2 7/21-1930 9 164-40.0 7/22-0015 98 164-07.2 7/22-0647 123
1.47 1.85	964		98 123	7/22-0015 98 7/22-0647 123 7/22-1510 2.8	164-40.0 7/22-0015 98 164-07.2 7/22-0647 123
1.85			123	7/22-0647 123 7/22-1510 2.8	164-07.2 7/22-0647 123
	264			7/22-1510 2.8	
0.04	264		2.8		163-05.7 7/22-1510 2.8
0.20	264		13	7/22-2000 13	163 - 43.6 $7/22 - 2000$ 13
3.46	334		182	7/23-0410 182	165-08.7 7/23-0410 182
5.13	334		270	270	270
0.38	334		20	7/23-0940 20	164-57.1 7/23-0940 20
0.84	334		44	44	44
0.74	334		39	39	39
0.65	334		34	34	34
0.08	358		4.1	7/23-1645 4.1	165-15 7/23-1645 4.1
0.32	358		10.5	10.5	10.5
0.28	358		14.1	14.1	14.1
3.75	264		250	7/23-0005 250	164-32.8 7/23-0005 250
0.66	264		44	7/23-0325 44	165-13.8 7/23-0325 44
0.045	264		3.2	7/23-0910 3.2	165-24 7/23-0910 3.2
0.225	264		15.3	7/23-2027 15.3	164-51.2 7/23-2027 15.3
	0.226 0.26 0.26 0.28 0.38 0.46 0.44 0.28 0.08 0.28 0.28 0.28 0.28 0.28 0.28	264     1.85       264     0.04       264     0.04       264     0.20       334     0.20       334     0.34       334     0.38       334     0.38       334     0.38       334     0.38       334     0.38       334     0.38       335     0.38       358     0.32       358     0.32       358     0.46       358     0.32       358     0.32       358     0.44       358     0.44       358     0.44       358     0.44       358     0.28       358     0.28       264     0.45       264     0.28       264     0.28       264     0.28	2.8 $264$ $0.04$ 13 $264$ $0.20$ 182 $334$ $5.13$ 270 $334$ $5.13$ 20 $334$ $5.13$ 20 $334$ $5.13$ 20 $334$ $0.26$ $44$ $334$ $0.38$ $41$ $334$ $0.38$ $34$ $0.334$ $0.084$ $314$ $0.38$ $0.28$ $4.1$ $358$ $0.28$ $14.1$ $358$ $0.28$ $14.1$ $358$ $0.28$ $14.1$ $358$ $0.28$ $14.1$ $358$ $0.28$ $15.0$ $264$ $0.666$ $3.75$ $0.466$ $3.75$ $15.3$ $264$ $0.045$ $15.3$ $264$ $0.28$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	

TABLE D.4 ANALYSIS OF SEA WATER SAMPLES, SHOT TEWA

and the state of the second of the second of the second of the second second second second second second second

おうちょうろうろう どうちょう ちょう

DOE ARCHIV

68

TABLE D.4 ANALYSIS OF DEPTH RAMPLES OF SEA WATER, SHOT TEWA Count time corrected to 1,000 hours.

1

A NAME AND ADDRESS OF A DESCRIPTION OF A

The second secon

3

-----

And the second s

----

state a state and state

;

•\_

Rate Latence Manue         Particue         Particue <th>,</th> <th></th> <th></th> <th></th> <th>WILLED OF 950 TH</th> <th></th> <th></th> <th></th> <th>z</th> <th>æ</th> <th>٤</th> <th>10<sup>3</sup> dis/min/liter</th> <th>10<sup>3</sup> dia/min/liter</th> <th>10<sup>2</sup> dia/min/lite</th>	,				WILLED OF 950 TH				z	æ	٤	10 <sup>3</sup> dis/min/liter	10 <sup>3</sup> dia/min/liter	10 <sup>2</sup> dia/min/lite
	Count	time corrected ti	01 002 0	Mrs.				T-5	12-11	165-10.5	0	42.0	170	212
N         K         m         Id         Id <th>Station</th> <th>i Latitude Lon</th> <th>ugitude</th> <th>Depth</th> <th>Particulate</th> <th>Salt</th> <th>Total</th> <th></th> <th></th> <th></th> <th>0</th> <th>25.0</th> <th>240</th> <th>265</th>	Station	i Latitude Lon	ugitude	Depth	Particulate	Salt	Total				0	25.0	240	265
		Z	4	E	10 <sup>1</sup> (dis/min)/liter	10 <sup>3</sup> (dis/min)/liter	10 <sup>1</sup> (dis/min)/liter				0	40.0	240	280
			, ;								0	36.6	270	306
	<b>P</b> -2	12-10 165-	-31.3	•	13	9.7	12				۸V	35.8	2.30	266
					0.0 2 at	5	06				80	15.0	250	265
					10.3	3 5	67 1				16	24.0	250	275
				0	4, 1	C.7	71				24	15.0	250	265
				Jav			07				32	24.0	250	274
				25	0.7	7	80				66	2.5	250	253
				50	3.0	4.4	7				51	18.0	195	213
				75	3.0	15	18				5	10.0	58	68
				06	0	0	0				62	1.3	12	61
				105	0	0	0				811	8.6	2.6	5.1
				125	0	7.3	7				158	2.5		5.5
				150	0	0	0				•	2		
14       14 <td< td=""><td></td><td></td><td></td><td>250</td><td>0</td><td>9</td><td>9</td><td>T-7</td><td>12-30.5</td><td>164.57.1</td><td>0</td><td>7.5</td><td>110</td><td>118</td></td<>				250	0	9	9	T-7	12-30.5	164.57.1	0	7.5	110	118
Note:       Note: <th< td=""><td></td><td></td><td></td><td>300</td><td>0</td><td>£</td><td>6</td><td></td><td></td><td></td><td>0</td><td>5.7</td><td>125</td><td>131</td></th<>				300	0	£	6				0	5.7	125	131
				500	0	0	0				•	3.7	125	129
		-					:				0	7.1	110	117
	8- <i>1</i>	12-07 164-	-52.3	0	5.3	22.5	87				N N	6.0	117.5	124
Net       Net       Net         100       10				11	11.5	42	30				-	151	130	145
				Aver			32				20	7.9	128	136
				25	3.8	20	24				30	2.5	130	133
10       10 <td< td=""><td></td><td></td><td></td><td>60</td><td>4.2</td><td>19</td><td>23</td><td></td><td></td><td></td><td>40</td><td>1.6</td><td>52.5</td><td>54</td></td<>				60	4.2	19	23				40	1.6	52.5	54
111       1				75	4.0	15	61				50	0.1	5.1	5.2
III       IIII       IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII				16	0.3	1.2	1.5				90	0.04	3.5	3.5
128       0       11 <td< td=""><td></td><td></td><td></td><td>106</td><td>0</td><td>0</td><td>0</td><td></td><td></td><td></td><td>10</td><td>0.02</td><td>1.1</td><td>1.1</td></td<>				106	0	0	0				10	0.02	1.1	1.1
11       1				126	0	0	0				80	0.07	2.0	2.1
25) 0.1 2.2 2. 2. 10 7.0 2.4 11.45 15.15.8 0 10 7.0 2.4 11.45 15.15.8 0 10 7.0 2.4 11.45 15.15.8 0 10 7.0 2.4 11.45 15.15.8 0 10 7.0 2.4 11.45 15.15.8 0 10 7.0 2.4 11.45 15.15.8 0 10 7.0 7.6 11.45 15.15.8 0 10 7.0 7.6 11.45 15.15.8 0 10 7.0 7.6 11.45 15.15 10.1 10 7.0 7.6 11.45 15.15 10.1 10.1 10.1 10.1 11.45 15.15 10.1 10.1 10.1 11.45 15.15 10.1 10.1 10.1 11.45 15.15 10.1 10.1 10.1 11.45 15.15 10.1 10.1 10.1 11.45 15.15 15.15 11.45 15.15 15.15 11.45 15.15 15.15 11.45 15.15 15.15 1				151	0.1	1.2	-				06	0.13	2.0	2.1
101       50       0.1       50       0.1       50       0.1         201       1.0       5       1.0       5       1.0       1.0       1.0         201       1.0       5       1.0       5       1.0       5       1.0       4         201       1.0       2.2       1.0       5       1.0       5       1.0       4         201       1.1       1.1       1.1       1.1       1.1       5       1.1       5				253	0.1	2.2	2				100	7.0	2.4	9.4
N-11       11-46.2       166.156       0       0       10       25       10       2       0       0       10       2       0       0       10       1       1       4       0       0       1       1       4       1       1       4       1       1       4       1       1       4       1       4       1       4       1       4       1       4       1       4       1       4       1       4       1       4       1       4       1       1       4       1       1       4       1       1       4       1       1       1       4       1 <th1< th="">       1</th1<>				351	0.1	5.0	s	é			4	01		44
Nrt       I.4.2       Iss.				201	0	0	0	B-1	2.66-11	C1-001		0.6	3	60
<b>DOE</b> AFCHAVE	N-17	11-46.2 165-	-15.6	6	45	185	230				~ c	3.6	46	20
DOE VECHANE 20 2.6 2.6 2.6 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7				10	22.2	101	123				• e	3.3	4	
DOE ARCHIVE				20	2.6	15.4	18				,			i
				30	1.1	8.8	10				۸V	2.5	49	51
DOC 315 110 111 1120 114 115 115 115 115 115 115 115				40	8.6	50	59				10	1.7	33	35
DOE 224 20 110 0.4 17 0				50	33.5	110	144				25	0.2	30	30
DOE VECHANE 10 0 0 0 12.6 13 10 0 0 0 12.6 13 10 0 12.6 13 10				60	18.6	120	139				40	4.7	67	72
DOE AFC 100 10 10 10 10 10 10 10 10 10 10 10 10		ī		70	11	30	41				45	5.4	56	61
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		D		90	0.B	2	2.6				50	15	105	120
00     <		C		()6	0.4	2	7.4				55	10.2	23.7	34
		Þ		100	0.4	2	2.4				60	12.6	611	161
											70	5.7	16.5	22
		A 1									85 1 0 0	7.0	13.5	21
		R.(						ę			001	0.4	1.6	с -
								•						
-, F														
		2 F												



Figure D.1 Gamma dose rate at 3 feet related to surface beta activity.

DOE ARCHIVES

Carley and a second second

Constraints of the second s



## REFERENCES

1. Merril Eisenbud and others; "Radioactive Debris from Operation Ivy"; NYO-4522, April 1953; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Secret Restricted Data.

2. A. Breslin and M. E. Cassidy; "Radioactive Debris from Operation Castle, Islands of the Mid-Pacific"; NYO-4623, January 1955; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Secret Restricted Data.

3. H.D. LeVine and R.T. Graveson; "Radioactive Debris from Operation Castle—Aerial Surveys Following Yankee-Nectar; NYO-4613; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Secret Restricted Data.

4. R.T. Graveson, M.E. Cassidy and S. Watnick; "Aerial Survey Techniques, Operation Wigwam"; Internal Report; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Secret Restricted Data.

5. J. Harley and N. Hallden; "Method of Calculating Infinite Gamma Dose from Beta Measurements on Gummed Film"; Laboratory Report 56-2; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Unclassified.

6. "Capabilities of Atomic Weapons"; Department of the Army Technical Manual TM 23-200, Department of the Navy OPNAV Instruction 03400.1B, Department of the Air Force AFL 136-1, Marine Corps Publications NAVMC 1104 Rev; Revised Edition November 1957; Prepared by Armed Forces Special Weapons Project, Washington, D.C.; Confidential.

7. H.F. Hunter and N.E. Ballou; "Simultaneous Slow Neutron Fission of U<sup>235</sup> Atoms. I. Individual and Total Rates of Decay of the Fission Products"; ADC-65, April 1949; U.S. Naval Radiological Laboratory, San Francisco, California; Unclassified.

8. Radiological Health Handbook, Page 250, October 1955; U.S. Department of Health, Education, and Welfare; Cincinatti, Ohio; Unclassified.

9. Feenan D. Jennings and others; "Fallout Studies by Oceanographic Methods"; Project 2.62a, Operation Redwing, ITR-1316, July 1956; University of California, Scripps Institution of Oceanography, La Jolla, California; Secret Restricted Data.

10. K. O'Brien, W. M. Lowder and L. R. Solon; "A Semi-Empirical Method of Calculating the Energy-Absorption Build-Up Factor with an Application to a Uniformly Contaminated Space Having Spherical Boundaries"; HASL-2, October 1957; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Unclassified.

11. M. E. Cassidy, R. T. Graveson and H. D. LeVine; "HASL Aerial Survey System"; NYO-2071, June 1957; Health and Safety Laboratory, U.S. Atomic Energy Commission, New York Operations Office; Unclassified.

H.D. LeVine and S. Watnick: "Portable Airborne Radiological Monitoring System";
 Project 32.2, Operation Plumbbob, WT-1463 (draft manuscript); Health and Safety Laboratory,
 U.S. Atomic Energy Commission, New York Operations Office; Unclassified.

DOE ARCHIVES




- Director, U.S. Naval Research Laboratory, Washington 25, D.C. ATTS: Mrs. Katherine E. Cass
   Commander, U.S. Naval Ordnance Laboratory, White Osk, 91- 92 Bilver Spring 19, Md.
  Director, Material Lab. (Code 900), New York Naval Shipyard, Brooklyn 1, N.Y. Commanding Officer and Director, Navy Electronics 94 Laboratory, Sar Diego 52, Calif. 95-98 Commanding Officer, U.S. Naval Radiological Defense Laboratory, San Francisco, Calif. ATTN: Tech. Info. Div. 99 Commanding Officer and Director, U.S. Naval Civil Engineering Laboratory, Fort Hueneme, Calif. ATIN: Code L31

   100 Superintendent, U.S. Naval Academy, Annapolis, Md.
   Commanding Officer, U.S. Naval Schools Command, U.S. Naval Station, Treasure Island, San Francisco, Calif. 101 President, U.S. Naval War College, Newport, Rhode Island 102 Superintendent, U.S. Neval Postgraduate School, Monterey, Calif. 103 Officer-in-Charge, U.S. Reval School, CEC Officers, U.S. Haval Construction Bn. Center, Fort Huename, Calif. 104 Commanding Officer, Nuclear Weapons Training Center, Atlantic, U.S. Naval Base, Norfolk 11, Va. ATTN: Nuclear Warfare Dept.
   105 Commanding Officer, Nuclear Weapons Training Center, Pacific, Naval Station, San Diego, Calif.
   Commanding Officer, U.S. Naval Danage Control Tng. Center, Naval Base, Philadelphia 12, Pa. ATIN: ABC Defense Course 107 Commanding Officer, Air Development Squadron 5, VI-5, China Lake, Calif. Commanding Officer, U.S. Naval Medical Research Institute, 108 National Naval Medical Center, Bethesda, Md. 109 Commander, U.S. Naval Ordnance Test Station, China Lake, Calif. 110 Officer-in-Charge, U.S. Nevel Supply Research and Development Facility, Neval Supply Center, Bayonne, N.J. 111 Commander-in-Chief, U.S. Atlantic Fleet, U.S. Naval Base, Norfolk 11, Va. 112 Commandant, U.S. Marine Corps, Washington 25, D.C. ATTN: Code A03E 113 Director, Marine Corps Landing Force, Development Center, MCS, Quantico, Va. 114 Chief, Bureau of Ships, D/N, Washington 25, D.C. ATTN: Code 372
   Commanding Officer, U.S. Naval CIC School, U.S. Naval Air Station, Clynco, Brunsvick, Ga.
   Tauri Omerations, Department of the Navy, Washin, 116 Chief of Neval Operations, Department of the Navy, Washing-ton 25, D.C. ATTN: OF-0985 117-119 Chief, Bureau of Naval Weapons, Navy Department, Washington 25, D.C. ATTN: RR12 120 Commander-in-Chief, U.S. Pacific Fleet, Fleet Post Office, San Francisco, Calif. AIR PORCE ACTIVITIES 121 Deputy Chief of Staff, Operations, BQ. USAF, Washington 25, D.C. ATTN: AFOOP 122 Hq. USAF, ATTN: Operations Analysis Office, Office, Vice Chief of Staff, Weshington 25, D. C.
  123 Director of Civil Engineering, Eq. USAF, Washington 25, D.C. ATTN: AFOCE-ES 124-134 Air Force Intelligence Center, HQ. USAF, ACS/I (AFCIN-3V1) Weshington 25, D.C. 135 Director of Research and Development, DCS/D, EQ. USAF, Washington 25, D.C. ATTN: Guidence and Wespons Div. 136 The Surgeon General, HQ. USAF, Washington 25, D.C. ATTN: Bio.-Def. Pre. Med. Division 137 Commander, Tactical Air Command, Langley AFB, Va. ATTN: Doc. Security Branch 138 Commander, Air Defense Command, Ent AFB, Coloredo. ATTN: Assistant for Atomic Energy, ADLOCA 139 Commander, Eq. Air Research and Development Command, Andrews AFB, Washington 25, D.C. ATTN: RDRWA

- 140 Commander, Air Force Ballistic Missile Div. BQ. ARD Force Unit Post Office, Los Angeles 45, Calif. AT.
- 141-142 Commander, AF Cambridge Research Center, L. G. Benso
- Laira
   Loringe research Cetter, L. S. Bensch
   Field, Bedford, Mess. ATTN: CRAST-2
   L43-L47 Commender, Air Force Special Wespons Center, Kirtler
   Albuquerque, N. Mer. ATTN: Tech. Info. & Intel. D:
   L48-L49 Director, Air University Library. Maxwell AFB, Ale.
  - Commander, Lovry Technical Training Center (TW), Lovry AFB, Denver, Coloredo.
     Commandant, School of Aviation Medicine, USAF, Aeris
    - Medical Center (ATC), Brocks Air Force Base, Tex. ATTN: Col. Gertit L. Hekhuis
- 152 Commander, 1009th Sp. Wpns. Squadron, HQ. USAF, Wash 25, D.C. 153-154 Commander, Wright Air Development Center, Wright-Pat
- Approx.
   Commander, wright Air Jevelopment Center, wright-Per AFB, Dayton, Ohio, WTN: WCAGT (For WOSC)
   155-156 Director, USAF Project RAND, VIA: USAF Liaison Offic The RAND Corp., 1700 Main St., Senta Monica, Call: Commander, 3525th Navigstor Wing, Mather AFB, Callin Commander, Air Defense Systems Integration Div., L. Hanacom AFB, Beddord, Mass. ATN: SIDE-S
   159 Commender Air Defense Systems Integration Div., L.

  - Commander, Air Technical Intelligence Center, USAF, Wright-Patterson AFB, Ohio, ATN: AFCIN-LBIA, Lib: Assistant Chief of Staff, Intelligence, H4, USAFE, 633, New York, N.Y. ATCN: Directorate of Air Targ 158
  - 159
  - Commander, Alaekan Air Command, APO 948, Seattle, Weshington, ATN: AAOTN Commander-in-Chief, Facific Air Forces, APC 953, Sa 160
  - 161 Francisco, Calif. ATTN: PFCIE-MB, Base Recovery

OTHER DEPARTMENT OF DEFENSE ACTIVITIES

- 162 Director of Defense Research and Engineering, Washi D.C. ATTN: Tech. Library
- 163
- Brecutive Secretary, Military Lisison Committee, Dept. of Defense, Washington 25, D. Committee, Director, Weapone Systems Evaluation ofoup, Room LE 164
- The Pentagon, Washington 25, D.C. 165 Commandant, The Industrial College of The Armed For
- Ft. McNair, Washington 25, D.C.
- 166 Commandant, Armed Forces Staff College, Norfolk 11, Ve. ATTN: Library 167-170 Chief, Defense Atomic Support Agency, Washington 25
  - ATTR: Document Library 171 Commander, Field Command, DASA, Sandia Base, Albuqu
    - N. Mei. 172 Commander, Field Command, DASA, Sandia Base, Albuqu
- N. Mex. ATTN: FCTG 173-174 Commander, Field Command, DASA, Sandia Base, Albuqu N. Mex. ATTN: FOWT
  - 175 Commander, JTF-7, Arlington Hall Station, Arlington 176 Commander-in-Chief, Strategic Air Command, Offutt A
  - Neb. ATTN: OAWS
  - 177 Commandant, DS Coast Guard, 1300 E. St., N.W., Wash 25, D.C. ATTN: Cdr B. E. Kilk.rst
    178 Commander-in-Chief, EUCOM, APO 125, New York, N.T. 179 Commander-in-Chief, Pacific, c/o Fieet Post Office, Francisco, Calif.

  - 180 U.S. Documents Officer, Office of the United States National Military Representative - SHAFE, APO 55, Rev York, N.Y.

## ATOMIC ENERGY COMMISSION ACTIVITIES

- 181-183 U.S. Atomic Energy Commission, Technical Library, 1 ton 25, D.C. ATTN: For DMA
   184-185 Los Alances Scientific Laboratory, Report Library,
- Box Madde Scientific Latintizy, Report Horary, Box 1663, Los Alacis, N. Mex. ATTN: Eelen Reuman Sandia Corporation, Classified Document Division, Base, Albuquerque, N. Mex. ATTN: E. J. Smyth, Jr University of Celifornia Lawrence Radiation Labore P.O. Box 508, Livermore, Calif. ATTN: Clovis G. 186-190
- 191-200
  - Weapon Data Section, Office of Sechnical Informatio 201 Extension, Oak Bidge, Tenn.
- 202-235 Office of Technical Information Extension, Oak Rid. Tenn, (Surplus)



DOE ARCHI

# DISTRIBUTION

### Military Distribution Category 26

#### ARMY ACTIVITIES

1

- 1 Deputy Chief of Staff for Military Operations, D/A, Washington 25, D.C. ATTN: Dir. of SW&R Chief of Research and Development, D/A, Washington 25, 2
- D.C. ATTN: Atomic Div.
- 3 Assistant Chief of Staff, Intelligence, D/A, Washington 25, D.C.
- Chief Chemical Officer, D/A, Washington 25, D.C.
- Chief of Englueers, D/A, Washington 25, D.C. ATTN: ENGNB Chief of Engineers, D/A, Washington 25, D.C. ATTN: ENGEB Chief of Engineers, D/A, Washington 25, D.C. ATTN: ENGEB
- à.
- 9- 10 Office, Chief of Ordnance, D/A, Washington 25, D.C. ATTN: ORDIN
  - Arist. Signal Officer, D/A, Research and Development Div., Washington 25, D.C. ATDN: SIGRD-4
     Chief of Transportation, D/A, Office of Planning and Int.,
  - Washington 25, D.C.
- The Surgeon General, D/A, Washington 25, D.C. ATTN: MEDNE 14 The Surgeon General, D/A, Washington cy, Dio. 1111.111
   17 Commanding General, U.S. Continental Army Command, Ft. . ղե
  - Monroe, Va. 18 Director of Special Weapons Development Office, Headquarters CONARC, Ft. Bliss, Tex. ATTN: Capt. Chester I. Peterson
  - 19 President, U.S. Army Artillery Board, Ft. Sill, Okla.
  - 20
  - President, U.S. Army Air Defense Board, Ft. Blies, Tex. President, U.S. Army Aviation Board, Ft. Rucker, Ala. ATTN: ATBG-DG 21
  - Commanding General, First United States Army, Governor's Island, New York 4, N.Y. 22
  - Commanding General, Second U.S. Army, Ft. George G. Meade, 23 Md. 24
  - Commanding General, Third United States Army, Ft. McPherson, Ga. ATTN: ACofS G-3 25
  - Commanding Ceneral, Fourth United States Army, Ft. Sam Houston, Tex. ATTN: G-3 Section Commanding Ceneral, Fifth United States Army, 1660 E. Hyde 26
  - Park Blvd., Ohicago 15, Ill. 27
  - Commanding General, Sixth United States Army, Presidio of San Francisco, San Francisco, Calif. ATTN: AMGCT-4 Commandant, Army War College, Carlisle Barracks, Pa. 28
  - ATTN: Library Commandant, U.S. Army Command & General Staff College, 29
  - Ft. Leavenworth, Kansas, ATTN: ARCHIVES Commandant, U.S. Army Air Defense School, Ft. Bliss, 30
  - Tex. ATIN: Command & Staff Dept. Commandant, U.S. Army Armored School, Ft. Knox, Ky. 31
  - Commandant, U.S. Army Artillery and Missile School, Ft. Sill, Okla. ATTN: Combat Development Department 32

  - Commandant, U.S. Army Aviation School, Ft. Rucker, Ala. Commandant, U.S. Army Infantry School, Ft. Benning, Ga. ATTN: C.D.S. 33 34
  - The Superintendent, U.S. Military Academy, West Point, 35
  - N.Y. ATTN: Prof. of Ordnance Commandant, The Quartermaster School, U.S. Army, Ft. Lee, Va. ATTN: Chief, QM Library Commandant, U.S. Army Ordnance School, Aberdeen Proving 36
  - 37 Ground, Md.
  - 38 Commandant, U.S. Army Ordnance and Guided Missile School, Redstone Arsenal, Ala.
  - Commanding General, Chemical Corps Training Comd., Ft. 39 McClellan, Ala. 40
  - Commandent, USA Signal School, Ft. Mormouth, N.J. Commandant, USA Transport School, Pt. Eustis, Va. ATTN: 41
  - Security and Info. Off. 42
  - Security and Info. Off. Commanding General, The Engineer Center, Ft. Belwoir, Va. ATTN: Asst. Cudt, Engr. School Commanding General, Army Medical Service School, Brooke Army Medical Center, Ft. Sam Houston, Tex. Director, Armsd Forces Institute of Pathilogy, Walter Reed Army Med. Center, 625 16th St., NW, Washington 25 D. 43

an a substantia a constantia de la constant

- ы,
- 25, D.C.
- 45 Commanding Officer, U. S. Army Research Lab., Ft. Enox, Ey.

- 46 Commandant, Walter Reed Army Inst. of Res., Walter
- Reed Army Medical Center, Washington 25, D.C. 47-48 Commanding General, Qm P&D Comd., QM R&D Cntr., Natick, Mass. ATTN: CBR Liaison Officer
- Commanding General, Qm. Research and Engr. Comd., USA, 49- 50 Natick, Mass.
- 51- 52 Commanding General, U.S. Army Chemical Corps, Research
- and Development Comd., Washington 25, D.C. 53-54 Commanding Officer, Chemical Warfare Lab., Army Chemical Center, Md. ATTN: Tech. Library
  - Commanding General, Engineer Research and Dev. Lab., 55 Ft. Belvoir, Va. ATTN: Chief, Tech. Support Branch 56 Director, Waterways Experiment Station, P.O. Box 631,
  - Vicksburg, Miss. ATTN: Library
- 57 Commanding Officer, Diamond Ord. Fuze Labs., Washington 25, D.C. ATTN: Chief, Nuclear Vulneratility Br. (230)
   58- 59 Commanding General, Aberdeen Proving Grounds, Md. ATTN:
  - Director, Ballistics Research Laboratory 60 Commanding Officer, Ord. Materials Research Off., Watertown Arsenal, Watertown 72, Mass.
  - ATIN: Dr. Foster 61 Commanding General, Ordnance Ammunition Command, Joliet,
  - T11.
  - 62 Commanding Officer, USA Signal R&D Laboratory, Bt. Monmouth, N.J.
  - Commanding General, U.S. Army Electronic Proving Ground, Ft. Buschuca, Ariz. ATTN: Tech. Library 63

  - 64 Commanding General, USA Combat Surveillance Agency, 1124 N. Highland St., Arlington, Va.
    65 Commanding Officer, USA, Signal R&D Laboratory, Ft. Monmouth, N.J. ATTN: Tech. Doc. Ctr., Evans Area
  - 66 Director, Operations Research Office, Johns Hopkins University, 6935 Arlington Rd., Betherda L4, Md. 67 Commandant, U.S. Army Chemical Corps, CBR Weapons School,
  - Dugway Proving Ground, Dugway, Utah.
  - 68 Commander-in-Chief, U.S. Army Europe, APO 403, New York, N.Y. ATTN: Opot. Div., Weapons Br.
  - Commanding General, Southern European Task Force, APO 69 168, New York, N.Y. ATTN: ACOTS G-3
  - Commanding General, Eighth U.S. Army, APO 301, San Francisco, Calif. ATTN: ACofS G-3 70
  - 71 Commanding General, U.S. Army Alaska, APO 949, Seattle, *dashington*
  - 72 Commading General, U.S. Army Caribbean, Ft. Amedor, Cenal Zone. ATTN: Cml Office
  - Commander-in-Chief, U.S. Army Pacific, APO 958, San Francisco, Calif. ATTN: Orinance Officer 73
  - Commanding General, USARFANT & MDPR, Ft. Brooke, 74 Puerto Rico
  - Commanding Officer, 9th Hospital Center, APO 180, Nev York, N.Y. ATTN: CO, US Army Nuclear Medicine 75 Research Detachment, Europe

## NATY ACTIVITIES

- 76-77 Chief of Naval Operations, D/N, Washington 25, D.C. ATTN: OP-03EG
  - 78 Chief of Naval Operations, D/N, Washington 25, D.C. ATTN: OP-75
  - Chief of Neval Operations, D/N, Washington 25, D.C. 79 ATTN: 0F-92202 Chief of Naval Personnel, D/N, Washington 25, D.C.
- 80 81- 82 Chief of Naval Research, D/N, Washington 25, D.C. ATTN: Code 811
- Chief, Bureau of Naval Weapins,  $\rm D/N$ , Washington 25, D.C. ATTN: DLI-3 83-85
  - 86 Chief, Bureau of Medicine and Surgery, D/N, Washington
    - 25, D.C. ATTN: Special Wprs. Def. Dir Chief. Bureau of Ordnance, D/N, Washin DOF ARCHIVE Chief, Bureau of Ships, D/N, Washington 25, D.C.
  - 88 ATTN: Code 423
  - 89 Chief, Bureau of Yards and Docks, D/N, Washington 25, D.C. ATTN: D-440

77

73